# "["

## Water Availability Analysis

Pridmore Property
General Plan Amendment P17-00135
Rezone P20-00223 and Use Permit P20-00222
Planning Commission Hearing May 15, 2024



# CMP Civil Engineering & Land Surveying Inc. 1607 Capell Valley Road Napa, CA 94558 (707) 266-2559 Cameron@CMPEngineering.com CMPEngineering.com



# Water Availability Analysis Report for the Pridmore Property (Formally Capell Valley School)

1191 Capell Valley Road

Napa, CA 94558

APN: 032-130-026

Prepared By:

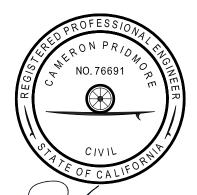
CMP Civil Engineering & Land Surveying Inc.

1607 Capell Valley Road

Napa, CA 94558

(707) 266-2559

Date: 2/9/2023



CMP Civil Engineering & Land Surveying Inc. - (707) 266-2559 - Cameron@CMPengineering.com

#### **Table of Contents**

Description	Page	
Title Page	1	
Table of Contents	2	
<ul> <li>Contact Information, Tier 1, 2 &amp; 3 WAA Analysis &amp; Summary</li> </ul>	3 - 4	
Attachment "A" Tier 1 Water Availability Analysis Support Documents	5 – 27	
• Attachment "B" Tier 2 Water Availability Analysis & Support Documents	28 – 47	
Attachment "C" Tier 3 Water Availability Analysis Documents	48 – 49	

CMP Civil Engineering & Land Surveying Inc. - (707) 266-2559 - Cameron@CMPengineering.com

Contact Inforn	Contact Information					
Property Owner:	Pridmore Family					
Owner Address:	1305 Capell Valley Road					
	Napa, CA 94558					
Owner Phone:	(707) 224-0682					
Contact:	Cameron Pridmore					
Contact Phone:	707-266-2559					
Contact Email	cameron@cmpengineering.com					

#### Site Map

Please see the Use Permit Site Plan for this project which has been included with this submittal for details and locations of proposed improvements. Below there is an included well location map which shows the existing water source (existing well) for this project and its proximity to other water sources.

#### Narrative

Up until a few years ago this 5 acre parcel located at 1191 Capell Valley Road was home to Capell Valley Elementary School. The school was open and in use for decades up until a few years ago when the district closed it and then recently sold the property to the Pridmores. The Pridmores are now proposing to install a maximum of 9 small tourist lodging units, 1 caretaker unit, 1 office/storage building and a barn type structure where local 4-H members could showcase a variety of their farming projects. Currently the property is served by a state approved small community water system (CA2800633) sourced by an existing well and 10,000 gallon storage tank. The said well is located on the general southeastern end of the property. See well location map below for the exact location. The well is currently used to provide potable water to the existing school buildings and has a capacity of 45 gallons per minute (GPM). Please see the well logs and other pertinent information included below. The well is currently fitted with a 55' deep seal with a minimum 3" annular space. The well water has been tested for adverse and hazardous constituents as required by local, state and federal permitting agencies. No constituents were found to be above allowable drinking water levels. There are only two neighboring wells within 500' of the subject parcels well. The first is 92' away and supplies water to the neighboring fire station. The second is 308' away and supplies water to an existing residence.

#### Tier 1 Analysis

Looking at the entire subject parcels water use and availability, the calculated historical elementary school water use for this parcel was 6.26 acre feet per year. The proposed calculated annual water use for this parcel is 3.20 acre feet. See the Water Availability Calculations included below. Given that this parcel is 5.08 acres in size and has a groundwater recharge rate of 0.98 acre feet of water per acre (see included Groundwater Recharge Calculations below) the maximum allowed water use for this parcel in a given year would be 4.98 acre feet of water per year. Onsite emergency water is available in the form of the existing 10,000 gallon water tank which will be utilized and if needed potable water will be hauled in from

CMP Civil Engineering & Land Surveying Inc. - (707) 266-2559 - Cameron@CMPengineering.com

the City of Napa or another public water system until repairs are made or a new well is installed. Please note that should there be an extreme emergency, such as a fire, there is an existing fire station right next store to the property which has multiple fire engines on hand at all times.

Comparing the proposed use of 3.20 acre feet per year to the above 4.98 acre feet value as well as the annual well capacity value of 72.59 acre feet per year, it is clear that the subject parcel and well has more than enough capacity to serve the proposed use. It is also clear that the proposed water use will be substantially less than what the calculated historical water use was. For further details please see the Tier 1 analysis support documents in Attachment A.

#### Tier 2 Analysis

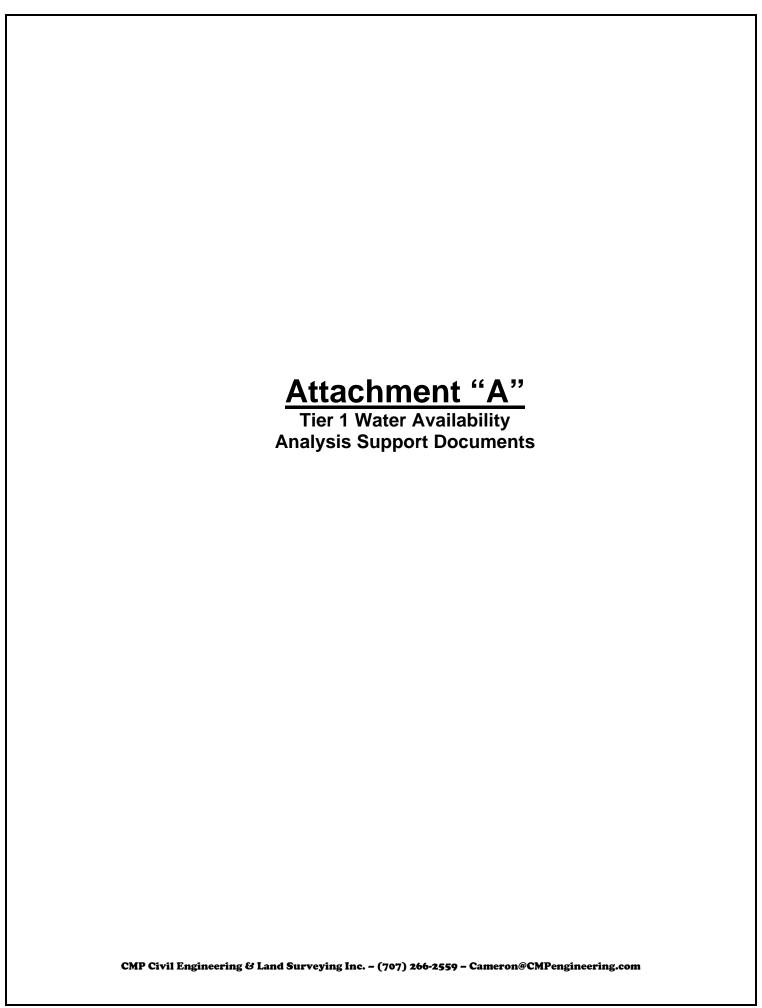
There are 2 neighboring wells within 500 feet of the project well listed in this report. One is 92 feet away and the other is 308 feet away. Because of this a Tier 2 well interference analysis was required to for this project. Attached to this report is the Tier 2 Water Availability Analysis prepared by Certified Engineering Geologist and Hydrogeologist David H. Peterson. In summary, the findings of this Tier 2 Analysis are as follows. The project well is expected to pump for a total of 66 minutes per day if pumping at its maximum yield of 43 GPM. Should the well pump for 66 minutes all at once (which is unlikely since it supplies water as needed throughout a given day) then it would draw down the well that is 92' away by only 1 foot. It would have little or no effect on the well that is 308' away. Further, a worst case scenario pumping event was considered. The estimated pump time was almost doubled to 120 minutes and it was found that the draw down on the 92' away well would be 8 feet and the draw down to the 308' well would be 2 feet. In both of these situation the drawdown on either neighboring well is less than 10 foot default well interference criteria for wells 6 inches in diameter or less as outlined in Appendix F-1 of the Napa County WAA Guidelines. Coupling this analysis with the fact that the well has been in service since 2006 when the school was operating at a much higher water demand along with the fact that during this time there were no reported adverse impacts to neighboring wells; it seems clear that the existing project well, operating at the lower proposed water demand, won't have a significant impact on any of its neighboring wells. For further details please see the said Tier 2 analysis in Attachment B.

#### Tier 3 Analysis

There are no significant streams within 1500 feet of the subject project, so a Tier 3 analysis is not necessary for this project. For further details see Tier 3 water availability documents in Attachment C.

#### Conclusion

In conclusion there is plenty of water onsite to support the proposed project. The proposed project will use significantly less water than the historical use. There is no significant impact to any neighboring wells. There is no impact to any significant streams. From a water standpoint there are no issues with this proposed project.





#### CMP Civil Engineering & Land Surveying Inc. 1607 Capell Valley Road Napa, CA 94558 (707) 266-2559 Cameron@CMPEngineering.com



## Water Availability Calculations for the Capell School Lodging Project

Located at: 1191 Capell Valley Road Napa, CA 94558

Date: 2/7/2023

Project # 00055

<u>Legend</u>
Requires Input
Automatically Calculates
Important Value Automatically Calculates
Important Value Requires Input

Hit ctrl+alt+shift+F9 when finished to recalc a

	—		
WATER USE CALCU			
RESIDENTIAL	#	FACTOR	AF/YR
PRIMARY RESIDENCES=	0	0.5	0.00
SECONDARY RESIDENCES=	0	0.2	0.00
FARM LBR DWELLING (# OF PPL) =	0	0.06 SUB TOTAL=	0.00
NON- PESID	ENTIAL CA	LCULATIONS	0.00
GRICULTURAL	# ACRE	FACTOR	AF/YR
VINEYARD IRRIGATION ONLY=	0	0.3	0.00
VINEYARD HEAT PROTECTION=	0	0.25	0.00
VINEYARD FROST PROTECTION=	0	0.25	0.00
IRRIGATED PASTURE=	0	4	0.00
ORCHARDS=	0	4	0.00
LIVESTOCK (SHEEP/COWS)=	0	0.01	0.00
( )	-	SUB TOTAL=	0.00
SCHOOL	# GAL	FACTOR	AF/YR
DOMESTIC WATER USE =	345379	SEE WW CALC	1.06
LANDSCAPING WATER USE =	1694310	SEE IRR. CALC	5.20
		SUB TOTAL=	6.26
NDUSTRIAL	# EMPL	FACTOR	AF/YR
FOOD PROCESSING=	0	31	0.00
PRINTING/ PUBLISHING=	0	0.6	0.00
		SUB TOTAL=	0.00
COMMERCIAL	# EMPL	FACTOR	AF/YR
OFFICE SPACE=	0	0.01	0.00
WAREHOUSE=	0	0.05	0.00
		SUB TOTAL=	0.00
EXIS	TING USE TO	OTALS	
RESIDENTIAL=	0.00	AF/YR	
AGRICULTURAL=	0.00	AF/YR	
SCHOOL=	6.26	AF/YR	
INDUSTRIAL=	0.00	AF/YR	
COMMERCIAL=	0.00	AF/YR	
OTHER USAGE (LIST BELOW)		, = 5	
RECYCLED WASTE WATER =		AF/YR	
		AF/YR	
TOTAL EXISTING WATER USE=	2039688	G/YR	
TOTAL EXISTING WATER USE=	6.26	AF/YR	

WELL NUMBER 1		IS FOR HIST	
1	Q - GPM	AF/YR	
	45	72.590	
2		0.000	
3		0.000	
4		0.000	
5		0.000	
TOTAL=	45	72.590	
SPRING NUMBER	Q - GPM	AF/YR	
1		0.000	
2		0.000	
3		0.000	
4		0.000	
5		0.000	
TOTAL=	0	0.000	
TANK #	GAL	AF	
1	10000	0.031	
2		0.000	
3		0.000	
4		0.000	
5		0.000	
TOTAL=	10000	0.031	
RESERVOIR #	GAL	AF	
1	0		
2	0		
3	0		
4	0		
5	0		
TOTAL=	0.000	0	
GROUND WATER RECHARGE	AF/YR/ACRE		AF/YR
See Groundwater Recharge Analysis	0.98	5.08	4.98
TOTAL AVAILABLE WATER =	1622106.10	G/YR	
IUIAL AVAILABLE WATER =	4.98	AF/YR	
TOTAL AVAILABLE WATER =	4.30		
	6.26	AF/YR	

WATER USE CALCULATIONS FOR PROPOSED USE							
RESIDENTIAL	#	FACTOR	AF/YR				
PRIMARY RESIDENCES=		0.5	0.00				
SECONDARY RESIDENCES=		0.2	0.00				
FARM LBR DWELLING (# OF PPL) =		0.06	0.00				
,		SUB TOTAL=	0.00				
NON- RESI	DENTIAL CAL	CULATIONS					
AGRICULTURAL	# ACRE	FACTOR	AF/YR				
VINEYARD IRRIGATION ONLY=		0.3	0.00				
VINEYARD HEAT PROTECTION=		0.25	0.00				
VINEYARD FROST PROTECTION=		0.25	0.00				
IRRIGATED PASTURE=		4	0.00				
ORCHARDS=		4	0.00				
LIVESTOCK (GOATS/CHICKENS)=	0.1	0.01	0.00				
		SUB TOTAL=	0.01				
LODGING	# GAL	FACTOR	AF/YR				
DOMESTIC WATER USE =	289988	SEE WW CALC	0.89				
LANDSCAPING WATER USE =	749406	SEE IRR. CALC	2.30				
		SUB TOTAL=	3.19				
INDUSTRIAL	# EMPL	FACTOR	AF/YR				
FOOD PROCESSING=	0	31	0.00				
PRINTING/ PUBLISHING=	0	0.6	0.00				
		SUB TOTAL=	0.00				
COMMERCIAL	# EMPL	FACTOR	AF/YR				
OFFICE SPACE=	0	0.01	0.00				
WAREHOUSE=	0	0.05	0.00				
		SUB TOTAL=	0.00				
PROP	OSED USE T	OTALS					
RESIDENTIAL=	0.00	AF/YR					
AGRICULTURAL=	0.01	AF/YR					
LODGING=	3.19	AF/YR					
INDUSTRIAL=	0.00	AF/YR					
COMMERCIAL=	0.00	AF/YR					
OTHER USAGE (LIST BELOW)							
RECYCLED WASTE WATER =		AF/YR					
		AF/YR					
		AF/YR					
		AF/YR					
		AF/YR					
	4040050	CAND					
	1042652	G/YR AF/YR					
TOTAL PROPOSED WATER USE= TOTAL PROPOSED WATER USE=	3.20						

WELL NUMBER         Q - GPM         AF/YR           1         45         72.590           2         0.000           3         0.000           4         0.000           5         0.000           5         0.000           SPRING NUMBER         Q - GPM         AF/YR           1         0.000           2         0.000           3         0.000           4         0.000           5         0.000           TOTAL=         0         0.000           TANK#         GAL         AF           1         10000         0.031           2         0.000         0.000           3         0.000         0.031           2         0.000         0.031           3         0.000         0.031           RESERVOIR#         GAL         AF           1         0         0           2         0         0           3         0         0           4         0         0           5         0         0           6         0         0           7 <th>WATER AVAILABILTY C</th> <th>ALCULATIO</th> <th>NS FOR PRO</th> <th>POSED (</th> <th>JSE</th>	WATER AVAILABILTY C	ALCULATIO	NS FOR PRO	POSED (	JSE
2 0.000 3 0.000 4 0.000 5 0.000 5 0.000	WELL NUMBER	Q - GPM	AF/YR		
3	1	45	72.590		
4 0.000 5 0.000 TOTAL= 45 72.590  SPRING NUMBER Q - GPM AF/YR 1 0.000 2 0.000 3 0.000 4 0.000 5 0.000  TOTAL= 0 0.000  TANK # GAL AF 1 10000 0.031 2 0.000 3 0.000 4 0.000  TOTAL= 10000 0.031  2 0.000  A 0.000  FOTAL= 10000 0.031  RESERVOIR # GAL AF 1 0 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	2		0.000		
5       0.000         TOTAL=       45       72.590         SPRING NUMBER       Q - GPM       AF/YR         1       0.000       0.000         2       0.000       0.000         3       0.000       0.000         5       0.000       0.000         TANK #       GAL       AF         1       10000       0.031         2       0.000       0.000         3       0.000       0.000         4       0.000       0.031         RESERVOIR #       GAL       AF         1       0       0         2       0       0         3       0       0         4       0       0         5       0       0         3       0       0         4       0       0         5       0       0         3       0       0         4       0       0         5       0       0         3       0       0         4       0       0         5       0       0         6       0 </td <td>3</td> <td></td> <td>0.000</td> <td></td> <td></td>	3		0.000		
TOTAL	4		0.000		
SPRING NUMBER         Q - GPM         AF/YR           1         0.000           2         0.000           3         0.000           4         0.000           5         0.000           TANK #         GAL         AF           1         10000         0.031           2         0.000         0.000           3         0.000         0.031           RESERVOIR #         GAL         AF           1         0         0.000           3         0         0.000           FOTAL=         0         0.000           3         0         0.000           4         0         0.000           5         0         0.000           GROUND WATER RECHARGE         AF/YR/ACRE         PARCEL AC         AF/YR           See Groundwater Recharge Analysis         0.98         5.08         4.98           TOTAL WATER AVAILABLE =         1622106.10         G/YR           TOTAL WATER AVAILABLE =         4.98         AF/YR           TOTAL PROPOSED WATER USE=         3.20         AF/YR	5		0.000		
1 0.000 2 0.000 3 0.000 4 0.000 5 0.000  TOTAL= 0 0.000  TANK # GAL AF 1 10000 0.031 2 0.000 3 0.000 3 0.000 4 0.000 5 0.000 3 0.000 4 0.000 5 0.000 5 0.000  TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 0.000  TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	TOTAL=	45	72.590		
2 0.000 3 0.000 4 0.000 5 0.000 TOTAL= 0 0.000 TANK # GAL AF 1 10000 0.031 2 0.000 3 0.000 4 0.000 5 0.000 5 0.000 5 0.000 TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 2 0 0 3 0 0 5 0 0 6 0 0 7	SPRING NUMBER	Q - GPM	AF/YR		
3 0.000 4 0.000 5 0.000 TOTAL= 0 0.000 TANK # GAL AF 1 10000 0.031 2 0.000 3 0.000 4 0.000 5 0.000 5 0.000 TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 2 0 0 3 0 0 5 0 0.000 TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 0.000 GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	1		0.000		
4 0.000 5 0.000 TOTAL= 0 0.000 TANK # GAL AF 1 10000 0.031 2 0.000 3 0.000 4 0.000 5 0.000 5 0.000 5 0.000 TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 2 0 0 3 0 0 4 0 0 5 0 0 COUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	2		0.000		
TOTAL= 0 0.000  TANK # GAL AF  1 10000 0.031  2 0.000  3 0.000  4 0.000  5 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0  2 0 0.000  3 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 0.000  3 0 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR  TOTAL WATER AVAILABLE = 4.98 AF/YR  TOTAL PROPOSED WATER USE= 3.20 AF/YR	3		0.000		
TOTAL= 0 0.000  TANK # GAL AF  1 10000 0.031  2 0.000  3 0.000  4 0.000  5 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0  2 0 0.000  3 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 0.000  2 0 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR  TOTAL WATER AVAILABLE = 4.98 AF/YR  TOTAL PROPOSED WATER USE= 3.20 AF/YR			0.000		
TANK # GAL AF  1 10000 0.031 2 0.000 3 0.000 4 0.000 5 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 2 0 0 3 0 0 4 0 0 5 0 0 6 0 0					
1 10000 0.031 2 0.000 3 0.000 4 0.000 5 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF 1 0 0 2 0 0 3 0 0 4 0 0 5 0 0 6 0		0			
1 10000 0.031 2 0.000 3 0.000 4 0.000 5 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF 1 0 0 2 0 0 3 0 0 4 0 0 5 0 0 6 0	TANK #	GAL	AF		
3 0.000 4 0.000 5 0.000 TOTAL= 10000 0.031 RESERVOIR # GAL AF 1 0 0 2 0 0 3 0 0 4 0 0 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1	10000	0.031		
4 0.000 5 0.000  TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 2 0 0 3 0 0 4 0 0 5 0 0  TOTAL= 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	2		0.000		
5       0.000         TOTAL=       10000       0.031         RESERVOIR #       GAL       AF         1       0       0         2       0       0         3       0       0         4       0       0         5       0       0.000         GROUND WATER RECHARGE       AF/YR/ACRE       PARCEL AC       AF/YR         See Groundwater Recharge Analysis       0.98       5.08       4.98         TOTAL WATER AVAILABLE =       1622106.10       G/YR         TOTAL WATER AVAILABLE =       4.98       AF/YR         TOTAL PROPOSED WATER USE =       3.20       AF/YR	3		0.000		
TOTAL= 10000 0.031  RESERVOIR # GAL AF  1 0 0 2 0 0 3 0 0 4 0 0 5 0 0  TOTAL= 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	4		0.000		
RESERVOIR #         GAL         AF           1         0         0           2         0         0           3         0         0           4         0         0           5         0         0.000           GROUND WATER RECHARGE         AF/YR/ACRE         PARCEL AC         AF/YR           See Groundwater Recharge Analysis         0.98         5.08         4.98           TOTAL WATER AVAILABLE =         1622106.10         G/YR           TOTAL WATER AVAILABLE =         4.98         AF/YR           TOTAL PROPOSED WATER USE =         3.20         AF/YR					
1 0 0 2 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0		10000			
1 0 0 2 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RESERVOIR #	GAL	AF		
2 0 0 3 0 4 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0					
3 0 0 4 0 0 5 0 0 0.000	2				
4 0 0 5 0 0 0.000					
5 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR					
TOTAL= 0 0.000  GROUND WATER RECHARGE AF/YR/ACRE PARCEL AC AF/YR See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR					
See Groundwater Recharge Analysis 0.98 5.08 4.98  TOTAL WATER AVAILABLE = 1622106.10 G/YR  TOTAL WATER AVAILABLE = 4.98 AF/YR  TOTAL PROPOSED WATER USE= 3.20 AF/YR			0.000		
TOTAL WATER AVAILABLE = 1622106.10 G/YR TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR	GROUND WATER RECHARGE	AF/YR/ACRE	PARCEL AC	AF/YR	
TOTAL WATER AVAILABLE = 4.98 AF/YR  TOTAL PROPOSED WATER USE= 3.20 AF/YR	See Groundwater Recharge Analysis	0.98	5.08	4.98	
TOTAL WATER AVAILABLE = 4.98 AF/YR TOTAL PROPOSED WATER USE= 3.20 AF/YR					
TOTAL PROPOSED WATER USE= 3.20 AF/YR					
REMAINING AVAILABLE WATER = 1.78 AF/YR					
	REMAINING AVAILABLE WATER =	1.78	AF/YR		



#### CMP Civil Engineering & Land Surveying Inc. 1607 Capell Valley Road Napa, CA 94558 (707) 266-2559 Cameron@CMPEngineering.com



# Ground Water Recharge Analysis for the Capell School Lodging Project

Located at: 1191 Capell Valley Road Napa, CA 94558

Date: 2/7/2023

Project # 00055

<u>Legend</u>
Requires Input
Automatically Calculates
Important Value Automatically Calculates
Important Value Requires Input

Hit ctrl+alt+shift+F9 when finished.

GROUND WATER RECHARGE CALCULATIONS									
PAF	RCEL VARIA	BLES							
Parcel size =	5.08	ac							
Average annual rainfall (P) =	25.40	in (from Prism	2012 - 2021)						
Total parcel average rainfall volume =	10.75	ac-ft/yr							
FVADO	TD A NODID A	ION (E)							
	TRANSPIRA		Γ						
Surface Type	Area (ac)	E (ac-ft)							
Vineyard =	0.00	0.00							
Orchard =									
Hay =									
Other Crops =									
Impervous Surfaces onto Grassland =	0.72	0.00							
Totals =	0.72	0.00							
Native plants area =	4.36	ac							
•		coefficient							
Native plants estimated coefficient =	0.35								
Plant density =	80%	percent							
Native Plant Growth Cycle Factor =	0.70	factor	O ITDC value tue ve						
Grass refernce ETo =	47.04	` ·	8 ITRC value typ yr)						
Native plant ETc =	11.52	in							
Total annual native plant E	3.35	ac-ft							
Total annual native plant E =	3.33	ac-ii							
Total annual E for parcel =	3.35	ac- ft							
- 10101 a.m.uu. 2 101 pui 001 -	0.00								
	RUNOFF (R)								
Average runoff relief coefficient =	8%	%							
Average runoff soil coefficient =	6%	%							
Average runoff vegitation coefficient =	6%	%							
Average runoff surface coefficient =	8%	%							
9									
Total Runoff Coefficient =	28%	%							
Average annual rainfall =	10.75	ac-ft							
Runoff producing rainfall =	80%	%							
Total Annual Runoff (R) =	2.41	ac-ft							
ANNUAL GROUND WATE	R RECHARG	E STORAGE	(S) = P-(R+E)						
Total Annaul Precipitation (P) =	10.75	ac-ft							
Total Annual Runoff (R) =	2.41	ac-ft							
Total Annual Evapotranpiration (E) =	3.35	ac-ft							
Total Annual Ground Recharge (S) =	4.99	ac-ft							
Annual Recharge Rate Per Acre =	0.98	ac-ft / yr / ac							

#### IRRIGATION CALCULATIONS FOR THE CAPELL SCHOOL LODGING PROJECT - 7/22/2020 HISTORICAL LANDSCAPE WATER USE CALCULATIONS LAWN LANDSCAPE AREA = 63237.45 SF 0.00 SF MISC. LANDSCAPE PLANT AREA = DROUGHT RISISTANT LANDSCAPE AREA = 0.00 SF DISTRIBUTION UNIFORMITY = 0.85 RATIO AVERAGE ANNUAL WATER USAGE = 5.20 AF PROPOSED LANDSCAPE WATER USE CALCULATIONS LAWN LANDSCAPE AREA = 21780.00 SF MISC. LANDSCAPE PLANT AREA = 10890.00 SF

Zone 8 Monthly Evapotranspiration

AVERAGE ANNUAL WATER USAGE =

DISTRIBUTION UNIFORMITY =

DROUGHT RISISTANT LANDSCAPE AREA =

Sprinkler Irrigation Typical Year

IRRIGATION TRAINING AND RESEARCH CENTER, California Polytechnic State University, San Luis Obispo

Table includes adjustments for bare spots and reduced vigor

(Typical Year)

10890.00 SF

0.85 RATIO

2.30 AF

	January	February	March	April	May	June	July	August	Septembe	October	Novembe	Decembe	Annual
	inches	inches	inches	inches	inches	inches	inches	inches	inches	inches	inches	inches	inches
Precipitation	6.21	0.29	0.34	0.30	0.49	0.22	0.07	0.31	0.43	0.65	4.92	4.29	18.52
Grass Reference ETo	1.53	2.43	3.44	4.82	5.74	5.79	5.92	5.70	4.78	3.58	1.56	1.74	47.04
Adjusted Site Specific Values													
Precipitation Average (NCRSS)	11.40	0.53	0.62	0.55	0.90	0.40	0.13	0.57	0.79	1.19	9.03	7.88	34.00
Grass Eto (ITRC)	1.53	2.43	3.44	4.82	5.74	5.79	5.92	5.70	4.78	3.58	1.56	1.74	47.04
Irrigation water required after rain	0.00	1.90	2.82	4.27	4.84	5.39	5.79	5.13	3.99	2.39	0.00	0.00	36.51
Miscelaneous Landscape Plants (ITRC)	0.78	0.88	1.19	1.77	2.75	3.26	3.01	2.76	1.52	0.87	0.52	1.03	20.34
Irrigation water required after rain	0.00	0.35	0.57	1.22	1.85	2.86	2.88	2.19	0.73	0.00	0.00	0.00	12.64
Drought Resistant Landscape Plants (CMP)	0.59	0.66	0.89	1.33	2.06	2.45	2.26	2.07	1.14	0.65	0.39	0.77	15.26
Irrigation water required after rain	0.00	0.13	0.27	0.78	1.16	2.04	2.13	1.50	0.35	0.00	0.00	0.00	8.36



#### CMP Civil Engineering & Land Surveying 1607 Capell Valley Road Napa, CA 94558 (707) 815-0988 Cameron@CMPEngineering.com

**CMPEngineering.com** 



# Historical Wastewater Flow Calculations for the

Capell School Lodging Project

Located at: 1191 Capell Valley Road Napa, CA 94558

Date: 7/22/2020

Project # 00055

Legend

Requires Input

**Automatically Calculates** 

Important Value Automatically Calculate

Important Value Requires Input

Hit ctrl + alt + shift + F9 when finished to recalc all formulas

## **Historical Waste Flow Summary**

The subject property used to be a public school with a peak attendence of 90 students, 3 teachers, 2 part time aids and a part time grounds keeper. The calculated flows below are based on this.

Historical School Peak Don	nestic Was	te Flow	Calcula	ations				
Historical Student Peak S	tudent Don	nestic Wa	aste Flo	WS				
Estimated peak number of students attending =	90	#						
Peak wasteflow per student =	20.00	gal/day/st	:d					
Peak Student Waste Flow =	1800.00	gal/day						
Historical School Peak Employee Domestic Waste Flows								
Peak Employee Waste Flows								
Number of FT Employees =	3	#						
Number of PT Employees =	3	#						
FT employee daily domestic waste flow =	45.00	gal/day (1	5 g/p)					
PT employee daily domestic waste flow =	24.00	gal/day (8	3 g/p)					
Peak Employee Waste Flows =	69.00	gal/day						
		_						
Total Combined Domestic Waste Flows =	1869	gal/day						
Historical School Annual W	aste Flow	Volume	Calcula	ations				
Historical Student Aver	age Domes	stic Wast	e Flows					
Estimated peak number of students attending =	90	#						
Ave wasteflow per student =	10.00	gal/day/st	:d					
Ave Student Waste Flow =	900.00	gal/day						
Total Design Peak Domestic Waste Flows =	328500	gal/yr						
Historical Employee Ave	rage Dome	estic Was	ste Flow	S				
Peak Employee Waste Flows								
Number of FT Employees =	3	#						
Number of PT Employees =	2	#						
FT employee daily domestic waste flow =	22.50	gal/day (8	3 g/p)					
PT employee daily domestic waste flow =	8.00	gal/day (4	ł g/p)					
Total Dimestic Flow =	30.50	gal/day						
Total Design Peak Domestic Waste Flows =	11133	gal/yr						
Historical Average Eve	ent Domest	ic Waste	Flows					
Special Event Volumes	visitors	days/yr	flow/day	gallons				
Large Events =	200	4	5	4000				
Medium Events =	50	12	5	3000				
Other =			5	0				
Other 2 =			5	0				
Total Annual Event Visitor Waste Volume =	7000	gal/year						
Total Annual Waste Flow Volume =	346633	gal/yr	1.06	af				



#### CMP Civil Engineering & Land Surveying 1607 Capell Valley Road Napa, CA 94558 (707) 815-0988 Cameron@CMPEngineering.com

**CMPEngineering.com** 



# Proposed Wastewater Flow Calculations for the Capell School Lodging Project

Located at: 1191 Capell Valley Road Napa, CA 94558

Date: 7/22/2020

Project # 00055

Legend

Requires Input

Automatically Calculates

Important Value Automatically Calculate

Important Value Requires Input

Hit ctrl + alt + shift + F9 when finished to recalc all formulas

## **Waste Flow Summary**

The existing school wastewater system was under designed to handle a peak flow of 600 gallons per day of domestic wastewater. The proposed change in use will exceed this amount thus an additional wastewater system will be required. All proposed events will be serviced by portable toilets.

Peak Domestic Waste Flow Calculations									
Proposed Lodging Units Peak Domestic Waste Flows									
Total number of single bedroom lodging units =	4	lodging u							
Total number of double bedroom lodging units =	5	lodging u							
Total number of single bedroom caretaker units =	1	caretaker							
Peak wasteflow per lodging bedrooms =	106.00	gal/day/bi							
Peak wasteflow per care taker bedrooms =	120.00	gal/day/bi							
Peak Lodging Units Domestic Waste Flow =	1604.00	gal/day							
Proposed Employee Po	eak Domes		e Flows						
Peak Employee Waste Flows									
Number of FT Employees =	4	#							
Number of PT Employees =	0	#							
FT employee daily domestic waste flow =	60.00	gal/day (1	5 g/p)						
PT employee daily domestic waste flow =	0.00	gal/day (8	3 g/p)						
Peak Employee Waste Flows =	60.00	gal/day							
Total Combined Domestic Waste Flows =	1664	gal/day							
Annual Waste Flow			ions						
Average Lodging Uni									
Total number of single bedroom lodging units =	4	lodging u							
Total number of double bedroom lodging units =	5	lodging units							
Total number of single bedroom caretaker units =	1	caretaker							
Total bedroom (br) count =	15	br	unito						
Average wasteflow per bedroom =	50.00	gal/day/bi	r						
Total Design Peak Domestic Waste Flows =	750.00	gal/day/bl							
Total Design Peak Domestic Waste Flows =	273750	gal/yr							
Average Employee			OWS						
Peak Employee Waste Flows	Domodio	racto i i	0110						
Number of FT Employees =	4	<b>]</b> #							
Number of PT Employees =	0	#							
FT employee daily domestic waste flow =	30.00	gal/day (7	7.5 g/p)						
PT employee daily domestic waste flow =	0.00	gal/day (4	• . ,						
Emplyee Domestic Flow =	30.00	gal/day	017						
Total Design Peak Domestic Waste Flows =	10950	gal/yr							
Average Event D	omestic Wa		VS						
Special Event Volumes	visitors	days/yr	flow/day	gallons					
Large Events =	150	6	3	2700					
Medium Events =	60	12	3	2160					
Other =			3	0					
Other 2 =			3	0					
Total Annual Event Visitor Waste Volume =	4860	gal/year							
Total Annual Waste Flow Volume =	289560	gal/yr	0.89	af					

**ORIGINAL** File with DWR

STATE OF CALIFORNIA

## WELL COMPLETION REPORT Refer to Instruction Pamphlet

Page 1 of 1

No. e039625

Owner's Well No. 1-'06 \_, Ended 7/13/2006 Date Work Began 6/29/2006

Local Permit Agency Napa County Environmental Mgmt
Permit No. E06-01092 Permit Date 6/3 Permit Date 6/28/2006

	DWR	USE	ONLY		DO	1	TO	FI	LL.	IN_	
			ı			<u></u>	1_	L			ot
STATE WELL NO./ STATION NO.											
					1	1		Ī	1	][	
	LATIT	UDE				LON	GITL	IDE			
				L		L					
APN/TRS/OTHER											

I CHIEL ING.	Permit Date 0/20/2000							
	GEOLOGIC LOG	WELL OWNER						
ORIENTATION (	VERTICAL — HORIZONTAL — ANGLE — (SPECIFY)	Name ( No.) Well by Unified School District						
DEPTH FROM	DRILLING ROTARY FLUID BENTONITE	Mailing Address Mailing Avenue						
SURFACE	DESCRIPTION	<b>QBP08 QBANNA</b> 94558 <b>M</b>						
Ft. to Ft.	Describe material, grain, size, color, etc.	CITY STATE ZIP						
	54 BROWN CLAY	Address 1191 Capell Valley Road						
54	BO GREEN CLAY WITH SANDSTONE	City Napa CA						
80 2	50 90% SANDSTONE/ 10% SHALE	County Napa						
250 2	50 90% SHALE & CLAY/ 10% SANDSTONE	APN Book 032 Page 130 Parcel 026						
		Township Range Section						
		Latitude 1 1 DEG. MIN. SEC. DEG. MIN. SEC.						
		LOCATION SKETCH————————————————————————————————————						
ļ		NORTH ✓ NEW WELL						
<del>  </del>	<u> </u>	MODIFICATION/REPAIR						
<b></b>		CAP Deepen						
		REEV - Other (Specify)						
		DESTROY (Describe						
,		DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG"						
		PLANNED USES (∠)						
<b></b>		WATER SUPPLY Domestic  Public						
	<u> </u>	SCHOOL SOMESTIC TO Public Ly Infigation Industrial						
		MONITORING —						
		WELL TEST WELL_						
		CATHODIC PROTECTION						
		HEAT EXCHANGE.						
		DIRECT PUSH						
		INJECTION						
		VAPOR EXTRACTION						
<del>  </del>		SPÁRGING						
<b></b>		Illustrate or Describe Distance of Well from Roads Buildings						
		Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.						
		WATER LEVEL & YIELD OF COMPLETED WELL						
		DEPTH TO FIRST WATER 70 (Ft.) BELOW SURFACE						
		DEPTH OF STATIC WATER LEVEL 15 (Ft.) & DATE MEASURED 7/13/2006						
		ESTIMATED YIELD * 45 (GPM) & TEST TYPE AIR LIFT						
TOTAL DEPTH O		TEST LENGTH 3 (Hrs.) TOTAL DRAWDOWN N/A (FL)						
TOTAL DEPTH C	F COMPLETED WELL 250 (Feet)	May not be representative of a well's long-term yield.						

	PTH	BORE.		CASING (S)						DEPTH			ANNULAR MATERIAL				
FROM St		BORE - HOLE DIA. (Inches)	BLANK	-	-NOS		MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	FRO		JRFACE o Ft.	CE- MENT	BEN- TONIT		/PE FILTER PACK (TYPE/SIZE)
0	260	12	60	ၓ	Ē	ᆵ		(inches)	ITICKNESS	(Inches)	-	0	5	<b>√</b>	<u>(₹)</u>	<u>(₹)</u>	CONCRETE
												5	22		1		GROUT
0	70		<b>V</b>				PVC F480	6	SDR-21			22	55	1			CEMENT
70	170			<b>√</b>			PVC F480	6	SDR-21	.032		55	250			1	#6 SAND
170	190		~				PVC F480	6	SDR-21								
190	250			1			PVC F480	6	SDR-21	.032							

UMBER

#### DAVE BESS PUMP & WELL

LIC.# C-57-C-10 487027

WATER WELL TEST REPORT# W-17-039 1115 MT GEORGE AVE. NAPA, CALIF. 94558 707-226-2539 / 253-0574

LOCATION (well address):	1191 Capell Valley Rd	Napa CA	Date	05Oct2017
TEST REQUESTOR:	Gil Pridmore			

#### SURFACE INSPECTION

CASING DIA. 6" pvc EST. AGE OF WELL 12 Years (Per Well Log) DEPTH OF WELL 250' (Per Well Log) SANITARY SEAL (functional) PIPING SYSTEM (functional) ELECTRICAL SYSTEM (functional) PRESSURE TANKS (functional) WELL SIZE OF PUMP 2 (HP)

OPERATING VOLTS: 239 AMPS: R: 2.8 B: 9.5 Y:P 10.0

#### FLOW TEST DATA

METHOD OF TEST: 2 HOUR OPEN FLOW DISCHARGE TEST USING THE INSTALLED PUMP AND EXISTING EQUIPMENT. (TEST EQUIPMENT USED), 2" FLOW METER, 2" THROTTLING DISCHARGE VALVE, 0/200 PRESSURE GAGE AND A POWERS WELL DEPTH STATIC METER.

TIME	RATE (GPM)	WATER LEVEL
14:00	50	20ft
15:20	43	56ft
15:40	43	61ft
16:00	43	61ft

STATIC LEVEL PRIOR TO TEST <u>20</u> FT STATIC LEVEL @ END OF TEST <u>61</u> FT TOTAL DRAW DOWN DURING THIS TEST WAS <u>41 ft</u> (AVG.)GALLONS PER MIN. <u>44.75</u> FOR <u>2</u> HOURS OF TESTING.

#### **GENERAL COMMENTS**

Well and well equipment in working order @ time of testing. The well fills a storage tank and is pressurized from the storage tank with 2 Goulds Booster pumps One ¾ HP (HB707) and 1 1hp (HB2510). Pressure Tanks are showing signs of deterioration (Rusting) and should be replaced. It seems that all controls are low voltage. The water is treated with a Culligan system, it is unknown if its operational or being serviced. Some information was taken from the well completion report Dated 6/28/2006 Log #e039625. Pump Depth is unknown at this time. Flow Meter Installed after the Booster pumps reads 5155799 Gallons.

Disclaimer: The data and conclusions provided herein are based upon the best information available to this company using standards and accepted practices of the water well drilling industry. However, well yield conditions are subject to dramatic changes in short periods of time due to usage and recharging of aquifers, etc. Therefore, the data and conclusions taken during this test are only valid of the day of the test and should not be relied upon to predict either the future quantity or quality of the well. This company makes no warranties either expressed or implied as to future water production and expressly disclaims and excludes any liability for consequential or incidental damages arising out of the breach of any expressed or implied warranty of future water production or out of any future use reported by the customer.

#### NELAP/ORELAP Certification 4036



Thursday, March 29, 2018

Gil Pridmore Pridmore Bros. Inc. 1191 Capell VAlley Napa, CA 94558

Re

Lab Order:

T030808

Project ID:

CAPELL SCHOOL

Collected By: GIL PRIDMORE

PO/Contract #:

PD MC \$345.00

Dear Gil Pridmore:

Enclosed are the analytical results for sample(s) received by the laboratory on Thursday, March 15, 2018. Results reported herein conform to the most current NELAC standards, where applicable, unless otherwise narrated in the body of the report.

If you have any questions concerning this report, please feel free to contact me.

**Enclosures** 

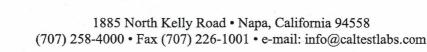
3/29/2018 14:04

REPORT OF LABORATORY ANALYSIS This report shall not be reproduced, except in full,

without the written consent of CALTEST ANALYTICAL LABORATORY

Page 1 of 4









#### **ENVIRONMENTAL ANALYSES**

#### **SAMPLE SUMMARY**

Lab Order:

T030808

Project ID:

**CAPELL SCHOOL** 

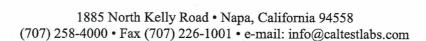
Lab ID	Sample ID	Matrix	Date Collected	Date Received
T030808001	CAPELL SCHOOL WELL HEAD	Water	03/15/2018 12:07	03/15/2018 13:01

3/29/2018 14:04

REPORT OF LABORATORY ANALYSIS This report shall not be reproduced, except in full,

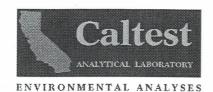
Page 2 of 4





without the written consent of CALTEST ANALYTICAL LABORATORY





### NARRATIVE

Lab Order:

T030808

Project ID: CAPELL SCHOOL

#### General Qualifiers and Notes

Caltest authorizes this report to be reproduced only in its entirety. Results are specific to the sample(s) as submitted and only to the parameter(s) reported.

Caltest certifies that all test results for wastewater and hazardous waste analyses meet all applicable NELAC requirements; all microbiology and drinking water testing meet applicable ELAP requirements, unless stated otherwise.

All analyses performed by EPA Methods or Standard Methods (SM) 20th Edition except where noted (SMOL=online edition).

Caltest collects samples in compliance with 40 CFR, EPA Methods, Cal. Title 22, and Standard Methods.

Dilution Factors (DF) reported greater than '1' have been used to adjust the result, Reporting Limit (RL), and Method Detection Limit (MDL).

All Solid, sludge, and/or biosolids data is reported in Wet Weight, unless otherwise specified.

Filtrations performed at Caltest for dissolved metals (excluding mercury) and/or pH analysis are not performed within the 15 minute holding time as specified by 40CFR 136.3 table II.

Results Qualifiers: Report fields may contain codes and non-numeric data correlating to one or more of the following definitions:

ND - Non Detect - indicates analytical result has not been detected.

RL - Reporting Limit is the quantitation limit at which the laboratory is able to detect an analyte. An analyte not detected at or above the RL is reported as ND unless otherwise noted or qualified. For analyses pertaining to the State Implementation Plan of the California Toxics Rule, the Caltest Reporting Limit (RL) is equivalent to the Minimum Level (ML). A standard is always run at or below the ML. Where Reporting Limits are elevated due to dilution, the ML calibration criteria has been met.

J - reflects estimated analytical result value detected below the Reporting Limit (RL) and above the Method Detection Limit (MDL). The 'J' flag is equivalent to the DNQ Estimated Concentration flag.

E - indicates an estimated analytical result value.

B - indicates the analyte has been detected in the blank associated with the sample.

NC - means not able to be calculated for RPD or Spike Recoveries.

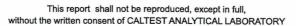
SS - compound is a Surrogate Spike used per laboratory quality assurance manual.

NOTE: This document represents a complete Analytical Report for the samples referenced herein and should be retained as a permanent record thereof.



#### REPORT OF LABORATORY ANALYSIS









Lab Order:

T030808

Project ID:

**CAPELL SCHOOL** 

**ANALYTICAL RESULTS** 

Lab ID

T030808001

Date Collected

3/15/2018 12:07

Matrix

Water

Sample ID CAPELL SCHOOL WELL

**HEAD** 

Date Received	3/15/2018 13:0

Parameters	Result Units	R. L.	DF Prepared	Batch	Analyzed	Batch	Qual
pH, Electrometric Analysis	Analytical Method:	SM 4500-H+ B-00/-	11		Analyzed by:	MYS	
рН	8.2 pH Uni	ts	1		03/25/18 14:48	BIO 19114	
Calculation, Hardness	Analytical Method:	Calculated			Analyzed by:	LM	
Hardness Calculation	33 mg/L	0.5	1		03/23/18 16:18	CALC	
Calculation, Total Anions	Analytical Method:	Calculated			Analyzed by:	DR	
Total Anions	4.3 meq/L		1		03/23/18 16:46	CALC	
Calculation, Total Cations	Analytical Method:	Calculated			Analyzed by:	LM	
Total Cations	4.5 meq/L		1		03/23/18 16:18		
Metals by ICPMS, Collision Mode, Total	Prep Method:	EPA 200.8			Prep by:	UKS	
	Analytical Method:	EPA 200.8			Analyzed by:	LM	
Arsenic	ND mg/L	0.00080	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Boron	3.6 mg/L	0.10	10 03/22/18 00:00	MPR 15782	03/26/18 16:44	MMS 8940	
Calcium	12 mg/L	2.0	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Iron	0.20 mg/L	0.10	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Magnesium	ND mg/L	2.0	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Manganese	0.013 mg/L	0.0020	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Potassium	ND mg/L	4.0	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Silica (as SiO2)	15 mg/L	4.0	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Sodium	88 mg/L	4.0	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Zinc	0.13 mg/L	0.080	4 03/22/18 00:00	MPR 15782	03/23/18 16:18	MMS 8940	
Electrical Conductance Analysis	Analytical Method:	SM 2510 B-97/-11			Analyzed by:	DR	
Conductivity	410 umhos/	cm 10	1		03/23/18 13:48	WET 9472	
Anions by Ion Chromatography	Analytical Method:	EPA 300.0			Analyzed by:	MYS	
Nitrogen, Nitrate (as N)	ND mg/L	0.1	1		03/16/18 01:29	WIC 6217	
Fluoride	0.35 mg/L	0.1	1		03/16/18 01:29	WIC 6217	
Chloride	7.8 mg/L	1	1		03/16/18 01:29	WIC 6217	
Sulfate (as SO4)	ND mg/L	0.5	1		03/16/18 01:29	WIC 6217	
Alkalinity, Total by Standard Methods	Analytical Method:	SM 2320 B-97/-11			Analyzed by:	DR	
Alkalinity, Total (as CACO3)	204 mg/L	10	1		03/23/18 16:46		
Hydroxide (as OH)	ND mg/L	2	1		03/23/18 16:46		
Bicarbonate (as HCO3)	244 mg/L	12	1		03/23/18 16:46		
Carbonate (as CO3)	ND mg/L	6	1		03/23/18 16:46		

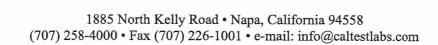
3/29/2018 14:04

#### **REPORT OF LABORATORY ANALYSIS** This report shall not be reproduced, except in full,

without the written consent of CALTEST ANALYTICAL LABORATORY

Page 4 of 4







The following information is from California Code of Regulations Title 22, Napa County Env. Health "Interpreting Drinking Water Test Results" and UC Davis Department of Land, Air, and Water Resources - Cooperative Extension. This information is provided for your convenience. Caltest does not provide consultation regarding the suitability of water for a given purpose.

Arsenic has a drinking water Maximum Contaminant Level (MCL) of 10 ug/L (ppb) or 0.010 mg/L (mqq)

Boron has an agricultural recommended limit and a state drinking water Action (Advisory) Limit of 1000 ug/L (ppb) or 1 mg/L (ppm). Boron affects the health and production of boron sensitive plants. Drinking water with greater than 10 times the Action Limit Level are recommended for removal from service.

Calcium and Magnesium are related to water hardness. See Hardness remarks.

Chloride has a drinking water Maximum Contaminant Level (MCL) of 600 mg/L, with a recommended level of 250 mg/L and a short-term limit of 600 mg/L.

Copper has a drinking water Maximum Contaminant Level (MCL) of 1000 ug/L (ppb) or 1 mg/L (ppm).

Electrical Conductance has a drinking water Maximum Contaminant Level (MCL) of 1,600 umhos/cm, with a recommended level of 900 umhos/cm and a short term limit of 2,200 umhos/cm. Electrical Conductance is a measure of the ability of a water to conduct an electrical current and is expressed in micromhos per centimeter at 25 degrees C.

Fluoride has a recommended level of 1.0 mg/L in temperate climates. Fluoride in concentrations greater than 3 mg/L can cause dental fluorosis (a brownish discoloration of the teeth).

Iron has a drinking water Maximum Contaminant Level (MCL) of 300 ug/L (ppb) or 0.3 mg/L (ppm).

Hardness is due primarily to calcium and magnesium carbonates and bi-carbonates. Up to 60 mg/L is SOFT. Between 60 to 120 mg/L is MODERATE (typically most desirable). Between 120 to 180 mg/L is HARD. Over 180 mg/L is VERY HARD.

Manganese has a drinking water Maximum Contaminant Level (MCL) of 50 ug/L (ppb) or 0.05 mg/L (ppm).

Sodium has a recommended limit of 100 mg/L. According to the American Heart Association, water containing more than 270 mg/L should not be consumed by those on a moderately restricted sodium diet.

Nitrate as N, has a drinking water Maximum Contaminant Level (MCL) of 10 mg/L. Nitrate as NO3 has a drinking water MCL of 45 mg/L.

Lead has a drinking water Action Limit of 15 ug/L (ppb) or 0.015 mg/L (ppm).

pH suggested level is 6.5 - 8.5.

Silica has a recommended limit of 70 mg/L. Silica in water may etch various household materials such as leaded crystal, marble, tile, windows, and porcelain.

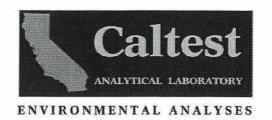
Sulfate has a drinking water Maximum Contaminant Level (MCL) of 500 mg/L, with a recommended level of 250 mg/L and a short term limit of 600 mg/L.

Zinc has a drinking water Maximum Contaminant Level (MCL) of 5000 ug/L (ppb) or 5 mg/L (ppm).

www.CaltestLabs.com

1885 N. Kelly Rd, Napa CA 94558 (707) 258-4000

Email: Info@CaltestLabs.com



#### Dear Client:

Caltest provides a variety of water analyses, but cannot provide an opinion regarding the quality of the water or its suitability for any particular use. If you would like information, please feel free to contact any of the following suggested resources listed below.

#### **Human Health Concerns:**

EPA Safe Drinking Water Hotline		800/426-4791
---------------------------------	--	--------------

Napa County Environmental Health 707/253-4471

Sonoma County Environmental Health 707/565-6565

#### **Irrigation Concerns:**

University of California at Davis

Department of Land, Air, and Water Resources/
Cooperative Extension. Ask for Blaine Hanson
or Steve Grattan

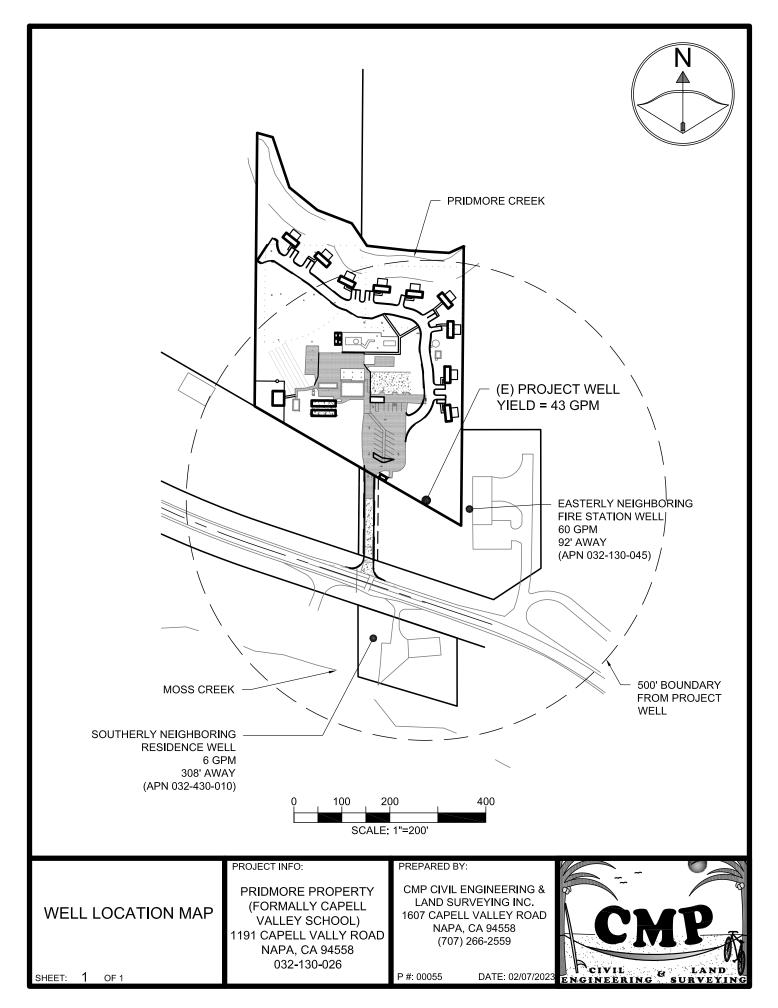
Thank you for choosing Caltest for your water testing needs. Please feel free to contact us if we can provide you with any further testing assistance.

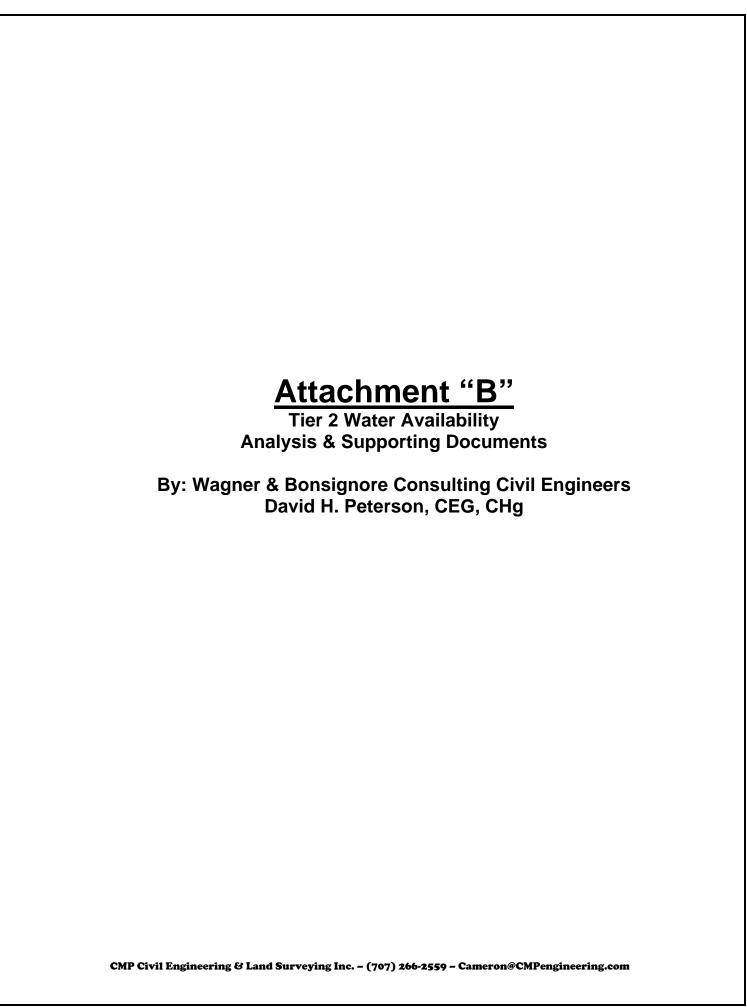
Sincerely, Caltest Analytical Laboratory

Todd M Albertson Vice President

(For your information, the next page contains various regulatory limits)

	1885 N. KELLY RC	AD • NAPA, CA 94558 •	(707) 258-4000	• Fax (70	7) 226-100	01 • www.	caltes	tlabs.com	m	LAB ORDER #:
Caltest	SAMPLECE	IAIN				P/	AGE	(	OF	tolknanx
ANALYTICAL LABORATORY	SAMPLE CH OF CUSTO	PROJECT #/	JECT NAME	oe/11	Sci	4000	) 		P.C	0.#
CLIENT: D 1		REPORT ATTN:	2.1	200	. a L			ANAL	YSES	REQUESTED
PridmoRa	O BROS	LNC DENN 10	Triciman e		011.00	11.11		_ /	//	TURN-AROUND
ADDRESS: 1905 Cape	Il Valley	Nava Ca	9455	8						TIME □ STANDARD
BILLING ADDRESS:	(7)		11				0/			RUSH
DUONE #	8104 SAMPL	ER (PRINT & SIGN NÄME): Gil Pridin	1014			Rockard				DUE DATE:
CALTEST DATE TIME SAMPLED MATRIX		IVE SAMPLE IDENTIFIC		CLIENT LAB#	COMP. or GRAB	20%/				REMARKS
3/15/1207		Capell School	, Well-trace							
							(	K. I O	N,	10, \$345.00
								/ / / / / / / / / / / / / / / / / / / /		4518
			, , , , , , , , , , , , , , , , , , ,							
			22							
										•
	,									
By submittal of sample(s), client	agrees to abide by th	e Terms and Conditions set	forth on the revers	se of this	iocument.	I magazasi		L		•
RELINQUISHED BY	DATECTIME	, RECEIVED I			IQUISHED E			DATE/T	IME	RECEIVED BY
sellace	3/15 17	or Colder								
				2						
Samples: WC   MICRO   B     BC   BIO   WC   MET     CC: AA   SV   VOA     SIL: HP   PT   QT   V   W/HNO,		VOA TEMP: 32°COMMENTS		/ N	INTACT:	<u>)</u> / N	DV C(	= Low R. V = Drinkin ONTAINE nber; PT =	L.s, Aque g Water; ER TYPI Pint (Pla	cous Nondrinking Water, Digested Metals; eous Nondrinking Water, Digested Metals; SL = Soil, Sludge, Solid; FP = Free Product ES: AL = Amber Liter; AHL = 500 ml stic); QT=Quart (Plastic); HG = Half Gallor
W/HNO, H,SO, NaOF										; B4 = 4 oz. BACT; BT = Brass Tube; VOA s ther Type Container
PIL: HNO,H,SO,NaOH	HCL									







Nicholas F. Bonsignore, P.E. Robert C. Wagner, P.E. Paula J. Whealen Martin Berber, P.E.
Patrick W. Ervin, P.E.
David P. Lounsbury, P.E.
Vincent Maples, P.E.
Leah Orloff, Ph.D, P.E.
David H. Peterson, C.E.G., C.H.G.
Ryan E. Stolfus

#### **MEMORANDUM**

**To:** Mr. Cameron Pridmore. P.E.

**From:** David H. Peterson, CEG, CHg

**Date:** February 8, 2023

**Re:** Tier 2 Water Availability Analysis

**Pridmore Family - Capell School Lodging Project** 

1191 Capell Valley Road, Napa, CA

This memorandum summarizes the Tier 2 water availability analysis performed for the proposed Capell School Lodging Project, located at 1191 Capell Valley Road, Napa, California. The property is located on the northeast side of Capell Valley Road and about 0.8 miles northwest of the intersection of Highways 121 and 128 in eastern Napa County, as shown on the attached *Site and Well Location Maps*, **Figures 1 and 2**.

A Tier 1 Water Availability Analysis (WAA) was performed by CMP Civil Engineering & Land Surveying Inc. (CMP) of Napa, California and summarized in a February 7, 2023 report. A copy of the *Well Location Map* from the CMP report is included as **Figure 3**. In that report, a project description and estimated water use were presented. Based on analysis of the project acreage, prior and planned water use, and guidelines presented in the County of Napa's Water Availability Analysis (WAA) – Guidance Document (dated May 12, 2015), the Tier 1 analysis concluded that annual recharge of 4.98 acre-feet per year (AFY) exceeded proposed water use of 3.20 AFY and so fell within allowable groundwater use guidelines. However, we understand that a Tier 2 analysis will be required by the County to assess the impacts of pumping by the project well on wells located within a 500-foot radius of project well.

#### **Project Description**

The subject property (Napa APN 032-130-026) is the site of the former Capell Valley School. The property slopes very slightly to the southwest, toward Oak Moss Creek. From review of the Tier 1 Water Availability Analysis by CMP (2023) and discussions with CMP, we understand that the planned project will consist of constructing up to nine small tourist lodging units, a caretaker unit, an office/storage building, and a barn-type structure for local 4-H events.

Water supply for the project will be from an existing well on the property, referred to as the Project Well. Total domestic and landscaping water demand for the project is calculated by CMP at 1,042,652 gallons per year, or 3.20 acre-feet per year (AFY). The estimated annual water

demand equates to about 2,857 gallons per day, or as will be discussed, about 66 minutes of daily pumping from the Project Well.

As part of the Tier 1 analysis, two offsite wells were identified within 500 feet of the Project Well (see *Well Location Map*, **Figure 3**); a well located 92 feet to the east at the Capell Valley Fire Department property (APN 032-130-045), and a domestic well located 308 feet to the southwest on a neighboring property (APN 032-430-010).

The purpose of our scope of services was to address the Tier 2 analyses required by the County of Napa. Our scope consisted of reviewing prior reports and plans for the project, available well completion reports, published geologic maps and groundwater reports for the site and vicinity; performing a site and area review; analyzing the data obtained; and preparing this memorandum. Subsurface investigation or well testing were not performed for the current scope. For project details, we relied primarily on the project description and water use estimates presented in the Tier 1 study by CMP (2023).

#### **Hydrogeologic Setting**

#### Geologic Units

The geologic setting in the vicinity of the site is shown on **Figure 4**, adapted from California Geological Survey (Delattre and Sowers, 2006) and our interpretation of the subsurface conditions is shown on Cross Section A-A' on **Figure 5**. As shown, the oldest mapped bedrock unit bounding and underlying the Capell Valley and subject property consists of a deformed mélange unit of the Jurassic- to Cretaceous-age Great Valley Sequence (map symbol *KJgvm*). This unit is described as consisting of fault-bounded, structurally disrupted mudstone, sandstone, shale and pebble conglomerate. While described as lithologically indistinguishable from more laterally continuous and less deformed strata in the Great Valley Sequence (unit *KJgv*), the mudstone in the mélange unit lacks bedding, while the sandstone and shale units are sheared and tightly folded. From the standpoint of groundwater storage and movement, flow through the highly sheared, faulted, and deformed mélange units of varying permeability is difficult to predict or model.

In the valley floor of Capell Valley, the deformed units of the Great Valley Sequence are blanketed by alluvial deposits, consisting of flat, relatively undissected fan, terrace and basin deposits of latest Pleistocene to Holocene age (Delattre and Sowers, 2006). Review of the well logs for the subject property and adjacent properties indicates that the alluvium ranges in thickness from about 38 feet in the adjacent properties, to about 54 feet in the Project Well. In general, the alluvium is described as consisting of brown clay, and brown clay with embedded rock. To the south of the subject property at APN 032-430-010, the alluvium also contains interbedded sandy clay and gravel.

#### Review of the Project Well Log

The well completion report (WCR e039625) for the Project Well is included as **Attachment 1**. The well was drilled in June-July 2006 by Huckfeldt Well Drilling Inc. of Napa, California. The initial wellbore (12-inch diameter) was drilled to a total depth of 260 feet by mud



rotary methods. The geologic log on the WCR indicates that alluvium consisting of brown clay was encountered to a depth of 54 feet. From a depth of 54 to 80 feet, green clay and sandstone are logged, that may be weathered bedrock, or sheared bedrock materials. Below 80 feet, "90% sandstone/10% shale" was encountered to 250 feet, underlain by "90% shale & clay/10% sandstone" to the bottom of the hole.

The wellbore was subsequently completed with a 250-foot deep, 6-inch (inside) diameter well casing. The well construction details indicate the well perforations extend from a depth of 70 to 170 feet and 190 to 250 feet, entirely within the Great Valley Sequence mélange unit. A bentonite and cement seal was placed in the upper 55 feet of the well, which extends through the surface alluvial units. Based on the reported 54-foot thickness of the alluvium on the log, it appears that the 55-foot well seal completely sealed off the alluvium from the underlying Great Valley Sequence bedrock units.

The WCR indicates that groundwater was first encountered at a depth of 70 feet in the boring, within the Great Valley Sequence. The static water level subsequently rose to a depth of 15 feet, indicating that groundwater is locally semi-confined or confined in the Great Valley Sequence bedrock. The well initially produced 45 gallons per minute during development, although the associated water level drawdown was not listed on the drillers report.

A well test was performed in 2017 by Dave Bess Pump & Well of Napa, California. A copy of that test is also included in **Attachment 1**. At the time of the testing in October 2017, the static water level in the well was 20 feet, somewhat lower than when first measured in July 2006. In the well test, the Project Well was pumped for two hours, at an initial rate of 50 gpm and later at 43 gpm. During the test, a total of 41 feet of pumping drawdown was recorded, indicating a specific capacity (the yield in gpm per foot of drawdown) of about 43gpm/41 ft drawdown = 1.05 gpm/ft drawdown. Based on the limited water level measurements presented on the test report, it appears that the water level in the well dropped for about 100 minutes and may have begun to level off after that time.

#### Tier 2 – Analysis of Well Pumping Interference

Pursuant to Appendix F of the WAA Guidelines, an evaluation of the approximate lateral extent of well pumping interference from the Project Well was performed. The Tier 1 WAA by CMP Engineering identified a well to the east on APN 032-130-045, located about 92 feet from Project Well. About 308 feet to the south, a well was identified on APN 032-430-010 (WCR 576432; see **Figure 3** for well locations and **Attachment 2** for well reports). The locations of the offsite wells were also verified on Google Earth aerial photography and during our site review.

Based on the method discussed in Driscoll (1986), the U.S. Geological Survey (Thomasson and others, 1960), and notes from the Groundwater Resources Association's *Low Yield Aquifer Testing* (2004) short course, the relationship between specific capacity and transmissivity was used to estimate the lateral pumping influence using information on the Well Completion Report for the Project Well and subsequent 2017 well test by Dave Bess Pump & Well. We used a procedure in



Driscoll (1986) based on the Cooper-Jacob straight-line method, which analyzes pumping drawdown vs. distance from the pumping well. An approximate relationship between specific capacity calculated from the 2017 well test and aquifer transmissivity was used, based on "typical" pump test values. As discussed above, the well was tested in 2017 at a discharge rate of 43 gallons per minute (gpm) with an associated measured drawdown of 41 feet, corresponding to a specific capacity of 1.05 gpm/ft drawdown.

The well completion report for the Project Well indicates that groundwater was first encountered at a depth of 70 feet and subsequently rose to static level of 15 feet indicating that groundwater in the bedrock (sandstone/shale) penetrated by the Project Well is likely confined and sealed off from the overlying unconfined alluvial aquifer. For our analysis, transmissivity was estimated for confined aquifer conditions, using the relationship of Specific Capacity (yield/drawdown) x 2,000, or 1.05 gpm/ft x 2,000 = 2,100 gallons per day/ft (gpd/ft). This relationship is presented both in Driscoll (1986) and Thomasson and others (USGS, 1960). This calculated transmissivity is higher than would be obtained using the County's hydraulic conductivity on Table F-4 of the WAA Guidelines (for Great Valley Sequence sandstone). Therefore, we consider the calculated transmissivity of 2,100 gpd/ft to be the more conservative estimate, as it would yield a larger potential extent of pumping impact.

To develop the slope of the drawdown curve to project away from the pumping well, the value of  $\Delta s$  (drawdown over one log graph cycle) was calculated for a distance-drawdown relationship, where  $T = 528Q/\Delta s$  (Driscoll,1986, Equation 9.11; where T = transmissivity and Q = pumping rate in gpm, or rearranged to solve for  $\Delta s = 528$  (43 gpm)/2,100 gpd/ft = 10.8.

Other assumptions in the calculation include adjusting the drawdown for the efficiency of the well. Frictional losses due to well screen size and sand pack can lead to reduced efficiency of the well (i.e., the water level in the formation outside of the well bore is higher than the level measured in the well). A properly designed, constructed, and developed well generally has an efficiency in the range of 70 to 80 percent (Driscoll, 1986; Rosco Moss Company, undated). Since the Project Well is newer, with factory-milled casing perforations, a higher efficiency of 80 percent was assumed.

The analysis is shown graphically on the attached semi-log plots (see **Attachment 3**). Using the estimated transmissivity of 2,100 gallons per day per foot of aquifer, pumping the project well at 43 gpm for 120 minutes under confined aquifer conditions would result in a zone of lateral pumping influence extending approximately 540 feet from the well. Under this scenario, the pumping influence would extend to the wells on both neighboring properties. It is estimated that at 120 minutes (the duration of the pumping test), the Project Well might cause about 8 feet of drawdown in the easterly well at APN 032-130-045 (Capell Fire Department), and about 2 feet of drawdown at the neighboring well to the south at APN 032-430-010. At these estimated drawdowns, effects to the neighboring wells would be within the allowable limit of the default well interference criteria (10 ft. for wells 6-inches in diameter or less) outlined in Appendix F-1 of the WAA Guidelines.



We also plotted the 2017 pump test data by Dave Bess Pump & Well as a time vs. drawdown relationship to assess the drawdown at the end of a typical project pumping cycle. After 66 minutes of pumping (the average daily project water demand at a rate of about 43 gpm), drawdown was estimated at 32 feet in the Project Well and 25.6 feet in the borehole wall (assuming 80 percent well efficiency). As shown on **Attachment 3** drawdown in the Project Well after 66 minutes would cause an associated drawdown of only about one foot at the Capell Fire Department well, and no measured drawdown in the southerly neighbor's well. However, the well pumps to a pressure tank and actual pumping cycles would likely be much shorter than 66 minutes. While these calculations are estimates, it should also be noted that the Project Well has been in operation since 2006 with no reported adverse impacts to neighboring wells.

#### **Discussion and Conclusions**

From the well logs, geologic maps and reports reviewed, and our analysis, groundwater pumping from the onsite Project Well under confined aquifer conditions appears to have a potential to influence two neighboring wells. Using the data from the Project Well log and 2017 well test data, we estimate that pumping the Project Well for 120 minutes would have an associated drawdown in the well at APN 032-130-045 (the Capell Valley Fire Station property) of about 8 feet. At the property to the south (APN 032-430-010), about 2 feet of drawdown was estimated. However, the effects after pumping for 66 minutes (the average daily project pumping demand) were estimated to amount to only about one foot of drawdown in the Capell Valley Fire Station well and little or no drawdown in the well at the property to the south. The analysis indicates that under both scenarios, effects would be within the allowable default values presented on Table F-1 of the County WAA Guidance Document.

We trust this memorandum provides the information requested by the County of Napa. Please contact us if you have questions about the findings or require additional information.

**Figures and Attachments** 

Figures 1 and 2 – Site and Location Map

Figure 3 – Well Location Map, from CMP Engineering (2023)

Figure 4 - Vicinity Geologic Map

Figure 5 – Cross Section A-A'

Attachment 1 – Onsite Well Log

Attachment 2 – Offsite Well Logs (2)

Attachment 3 – Well Pumping Interference Plots



#### References

California Department of Water Resources, 2020, Well Completion Report Map Application: <a href="https://dwr.maps.arcgis.com/apps/webappviewer/index.html?id=181078580a214c0986e2da28f86">https://dwr.maps.arcgis.com/apps/webappviewer/index.html?id=181078580a214c0986e2da28f86</a> 23b37

California Department of Water Resources, 2022, Water Data Library, online map application with groundwater level and water quality data: <a href="http://wdl.water.ca.gov/waterdatalibrary/">http://wdl.water.ca.gov/waterdatalibrary/</a>

CMP Civil Engineering & Land Surveying Inc., 2023, Water Availability Analysis Report for the Pridmore Property (Formally Capell Valley School), 1191 Capell Valley Road, Napa, CA 94558. APN 032-130-026: unpublished consultant's report dated February 7, 2023, 30p.

County of Napa, 2015, Water Availability Analysis (WAA) – Guidance Document: Adopted May 12, 2015, 42p.

Driscoll, F.G., 1986, Groundwater and Wells: Johnson Division, St. Paula Minnesota, 1,089p.

Groundwater Resources Association, 2004, Low Yield Aquifer Testing Seminar: notes from short course presented April 26, 2004, Walnut Creek, CA.

Johnson, A.I., Specific Yield – Compilation of Specific Yields for Various Materials in Hydrologic Properties of Earth Materials: U.S. Geological Survey Water-Supply Paper 1662-D, 80p.

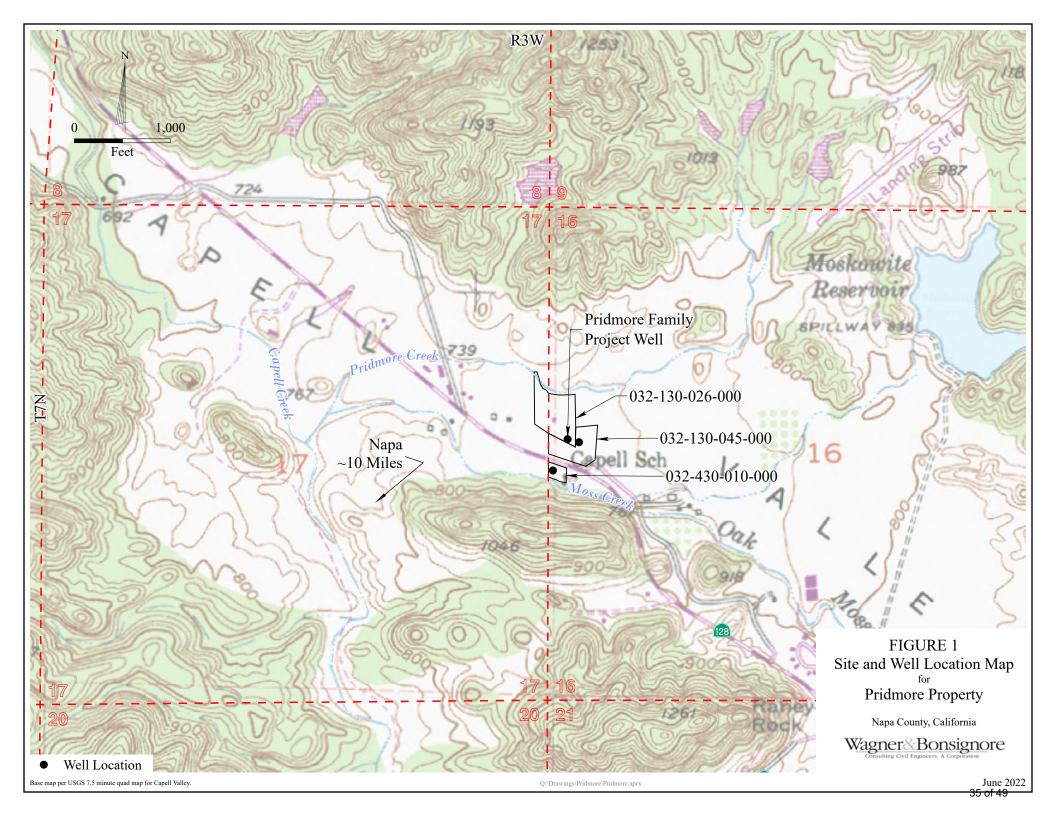
Kunkel, F. and Upson, J.E., 1960, Geology and Ground Water in Napa and Sonoma Valleys, Napa and Sonoma Counties, California: U.S. Geol. Survey Water-Supply Paper 1495, 252p., with illustrations.

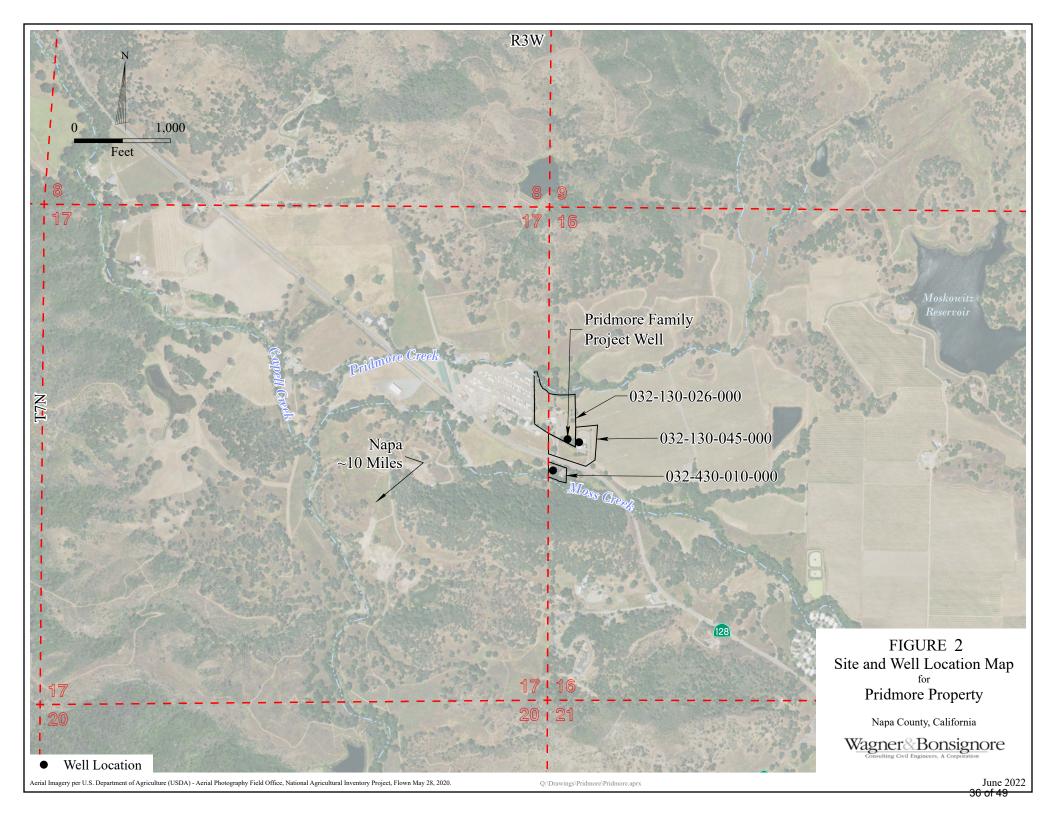
Rosco Moss Company, undated, Case Study; a Comparison of Well Efficiency and Aquifer Test Results Louvered Screen vs. Continuous Wire-Wrapped Screen, Big Pine, California: Technical Memorandum 004-1, 5p.

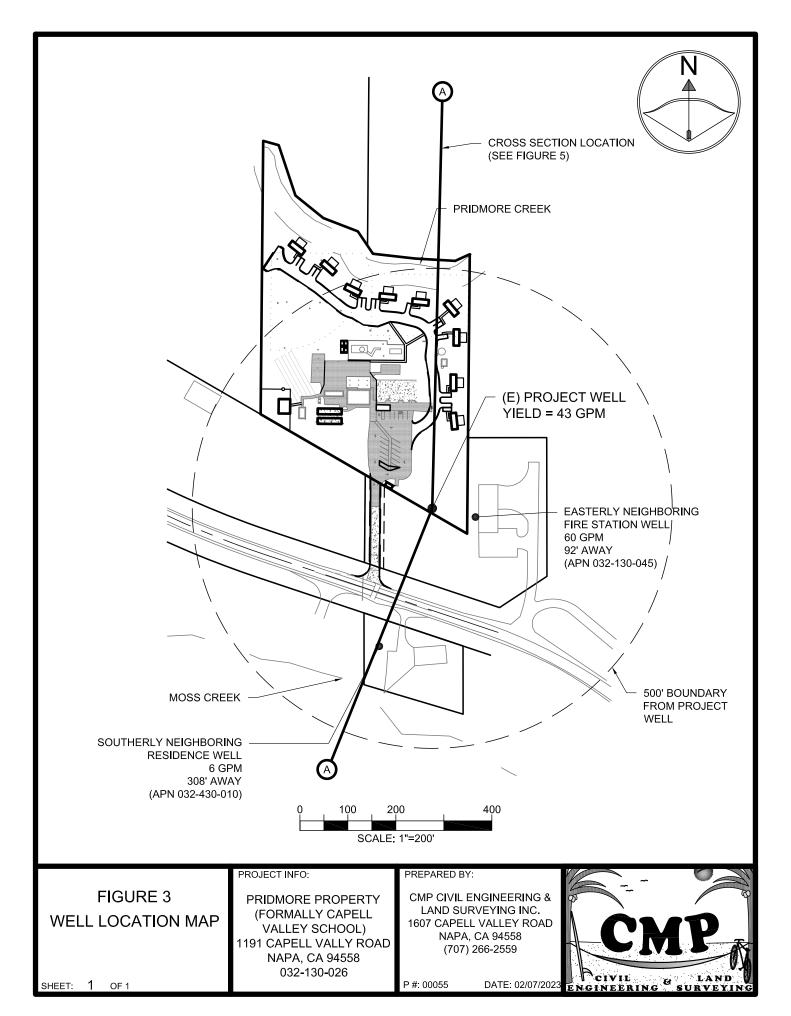
Thomasson, H.G., Olmsted, F.H., an LeRoux, E.F., 1960, Geology, Water Resources and Usable Ground-Water Storage Capacity of Part of Solano County, California: U.S. Geological Survey Water-Supply Paper 1464, 711p. (p.220-223; Hydraulic Characteristics Estimated from Pump-Efficiency Tests).

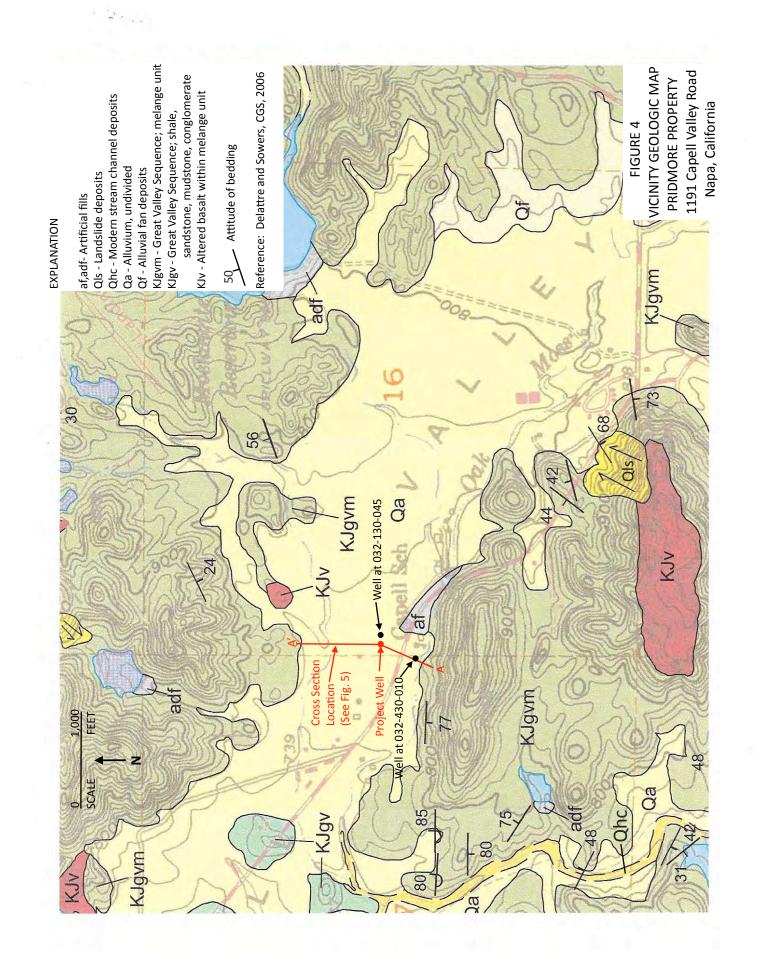
U.S. Geological Survey, 2022, National Water Information Service, online surface and groundwater data: <a href="https://waterdata.usgs.gov/nwis">https://waterdata.usgs.gov/nwis</a>











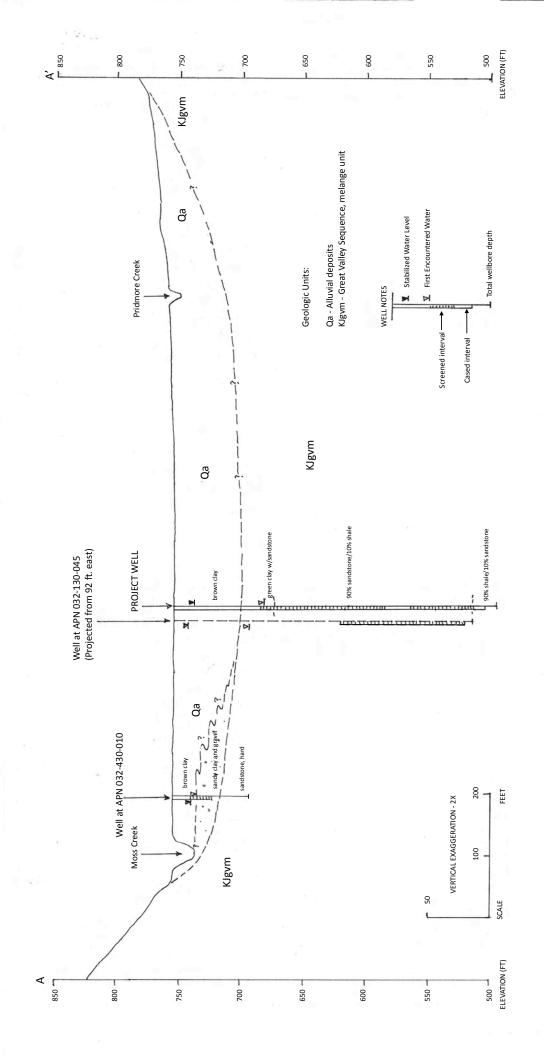


FIGURE 5 CROSS SECTION A - A' PRIDMORE PROPERTY 1191 Capell Valley Road Napa, California

### ATTACHMENT 1

**ORIGINAL** File with DWR STATE OF CALIFORNIA

WELL COMPLETION REPORT
Refer to Instruction Pamphlet

Page 1 of 1

Owner's Well No. 1-'06

No. e039625

, Ended 7/13/2006 Date Work Began 6/29/2006

Local Permit Agency Napa County Environmental Mgmt
Permit No. E06-01092 Permit Date 6/2

Permit Date 6/28/2006

STATE WELL NO./ STATION NO. LATITUDE LONGITUDE APN/TRS/OTHER

Perm	ut No. =	Permit Date 6/28/2006	
		GEOLOGIC LOG	WELL OWNER
ORIENTA	TION (≰)	VERTICAL HORIZONTAL ANGLE (SPECIFY)	
		DRILLING ROTARY FLUID BENTONITE	Mailing Address Mailingella Avenue
	FACE	DESCRIPTION	<b>Q3</b> Q3 <b>Q3 Q3 Q3 Q3 Q3 Q3 Q</b>
	o FL	Describe material, grain, size, color, etc.	CITY STATE ZIP
0		BROWN CLAY	Address 1191 Capell Valley Road
54	80	GREEN CLAY WITH SANDSTONE	City Napa CA
80	250	90% SANDSTONE/ 10% SHALE	County Napa
250	260	90% SHALE & CLAY/ 10% SANDSTONE	APN Book 032 Page 130 Parcel 026
i		We will be the second of the s	Township Range Section
			Latitude
			LOCATION SKETCH————————————————————————————————————
l			NORTH NEW WELL
l			MODIFICATION/REPAIR
<u> </u>			— Deepen — Other (Specify)
<b></b>			CREEK CREEK
			DESTROY (Describe
1			DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG"
			PLANNED USES (∠) WATER SUPPLY
			VATER SUPPLY Domestic _ Public
			SCHOOL SO Industrial
			MONITORING —
			WELL TEST WELL
			HEAT EXCHANGE.
			8 V DIRECT PUSH
			INJECTION
			VAPOR EXTRACTION
			SPARGING
			SOUTH REMEDIATION
	-		Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.
			WATER LEVEL & YIELD OF COMPLETED WELL
			DEPTH TO FIRST WATER 70 (Ft.) BELOW SURFACE
			DEPTH OF STATIC WATER LEVEL 15 (Ft.) & DATE MEASURED 7/13/2006
	1		ESTIMATED YIELD * 45 (GPM) & TEST TYPE AIR LIFT
		ORING 260 (Feet)	TEST LENGTH 3 (Hrs.) TOTAL DRAWDOWN N/A (FL)
TOTAL DE	PTH OF C	OMPLETED WELL 250 (Feet)	May not be representative of a well's long-term yield.

DEF		BORE.	CASING (S)									EPTH		ANNULAR MATERIAL				
FROM SU	FROM SURFACE HOLE DIA. (Inches)		T ¥	YPI	<u> (</u>	) JPE	MATERIAL /	INTERNAL DIAMETER	GAUGE OR WALL	SLOT SIZE IF ANY	FROM	SURF	ACE	CE-	BEN-		PE FILTER PACK	
Ft. to	FL	(mones)	BLANK	SCREEN	CON-	님	GRADE	(Inches)	THICKNESS	(Inches)	Ft	to	Ft.	MENT (✓)	TONITI	FILL ( <u>v</u> )	(TYPE/SIZE)	
0	260	12									0		5	✓			CONCRETE	
											5	; <u> </u>	22		1		GROUT	
0	70		<b>V</b>				PVC F480	6	SDR-21		22	! ]	55	✓			CEMENT	
70	170			<b>√</b>			PVC F480	6	SDR-21	.032	55	; ]	250			1	#6 SAND	
170	190		~	_			PVC F480	6	SDR-21			1						
190	250			1			PVC F480	6	SDR-21	.032		1						

ATTACHMENTS (∠)	I 7		- CERTIFICAT	ION STATEMENT -		<del></del>
Geologic Log	I, the undersigned, certify tha	t this report is	complete and accurate t	o the best of my knowledge and be	lief.	
Well Construction Diagram	NAME HUCKFELDT	WELL DRI	ILLING, INC.			
Geophysical Log(s)			(TYPED OR PRIN	TED)		
Soil/Water Chemical Analysis	2110 Penny Lane	11		Napa	CA	94559
Other	ADDRESS	Um K	14.6/1/4	CITY	STATE	ZIP
ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.	SignedWELL DRILLER/AU		TOPPESE TATIVE	07/14/06 DATE SIGNE		9-746 7 LICENSE NUMBER
	WELL DRILLERIAU	IMURIZED K	EPRESERIATIVE	DATE SIGNE	<i>u</i> ∪-o	I LICENSE NUMBER

# CAPELL SCHOOL WELL YIELD

#### DAVE BESS PUMP & WELL

LIC.# C-57-C-10 487027

WATER WELL TEST REPORT# W-17-039 1115 MT GEORGE AVE. NAPA, CALIF. 94558 707-226-2539 / 253-0574

LOCATION (well address):	1191 Capell Valley Rd	Napa CA	Date	05Oct2017
TEST REQUESTOR:	Gil Pridmore			

#### SURFACE INSPECTION

CASING DIA. 6" pvc EST. AGE OF WELL 12 Years (Per Well Log) DEPTH OF WELL 250' (Per Well Log) SANITARY SEAL (functional) PIPING SYSTEM (functional) ELECTRICAL SYSTEM (functional) PRESSURE TANKS (functional) WELL SIZE OF PUMP 2 (HP)

OPERATING VOLTS: 239 AMPS: R: 2.8 B: 9.5 Y:P 10.0

#### FLOW TEST DATA

METHOD OF TEST: 2 HOUR OPEN FLOW DISCHARGE TEST USING THE INSTALLED PUMP AND EXISTING EQUIPMENT. (TEST EQUIPMENT USED), 2" FLOW METER, 2" THROTTLING DISCHARGE VALVE, 0/200 PRESSURE GAGE AND A POWERS WELL DEPTH STATIC METER.

TIME	RATE (GPM)	WATER LEVEL
14:00	50	20ft
15:20	43	56ft
15:40	43	61ft
16:00	43	61ft

STATIC LEVEL PRIOR TO TEST <u>20</u> FT STATIC LEVEL @ END OF TEST <u>61</u> FT TOTAL DRAW DOWN DURING THIS TEST WAS <u>41 ft</u> (AVG.)GALLONS PER MIN. <u>44.75</u> FOR <u>2</u> HOURS OF TESTING.

#### **GENERAL COMMENTS**

Well and well equipment in working order @ time of testing. The well fills a storage tank and is pressurized from the storage tank with 2 Goulds Booster pumps One ¾ HP (HB707) and 1 1hp (HB2510). Pressure Tanks are showing signs of deterioration (Rusting) and should be replaced. It seems that all controls are low voltage. The water is treated with a Culligan system, it is unknown if its operational or being serviced. Some information was taken from the well completion report Dated 6/28/2006 Log #e039625. Pump Depth is unknown at this time. Flow Meter Installed after the Booster pumps reads 5155799 Gallons.

Disclaimer: The data and conclusions provided herein are based upon the best information available to this company using standards and accepted practices of the water well drilling industry. However, well yield conditions are subject to dramatic changes in short periods of time due to usage and recharging of aquifers, etc. Therefore, the data and conclusions taken during this test are only valid of the day of the test and should not be relied upon to predict either the future quantity or quality of the well. This company makes no warranties either expressed or implied as to future water production and expressly disclaims and excludes any liability for consequential or incidental damages arising out of the breach of any expressed or implied warranty of future water production or out of any future use reported by the customer.

## **ATTACHMENT 2**

# **Environmental**

**Cover Sheet** 

APN	032-130-045-000
Permit #	
Program	WEU.
DocType	WL
Street #	4193
Street Name	CAPELL VALLEY
Year	2000



For Loca Page 1	l Requir	ements		V	VELL C	COMPI Refer to Ins	struction Fa	N REP	ORT	BWR US	TATE WELL NO	اللا
Owner's					ded <b>9-2</b>	No.	747	744		LATITUDE		A THOUSE
Local P	к began <sub>-</sub> 'ermit Aøe	ency Na	pa O	, En ounty	Ged Environ	nmental	l Mont.					(31)
		96 <u>-1163</u> 6			Permit I				<del></del>		APN/TRS/	OTHER
ODIENTAT	10M ( 43)			IC LO	NTAL AI			Name		WELL (	WNER —	
		DRILLING			MTAL AI			Mailing Add	AC	7		
DEPTH SURF				DESC	CRIPTION			CITY CAN	7//			STATE ZIP
Ft. to					, grain size,			<del>-(\\\\</del>	<del>/ //</del>		CATION -	
20	<u>20</u> 38	prown	clay clay	MICE	enbedd	ed rock		Address City		HWY 128	<del></del>	
38	60	shale	& cl		22			County		Napa		
60	240	90% sa	<u>ndstr</u>	me/	10% sha	<u>le</u>		APN Book		Page 130		
	, .		23	<u> </u>		$\frac{\zeta}{\zeta}$				Range		
		7	<del>505</del>	X		////				NORTH SEC.		
		- 37/2								NORTH -		ACTIVITY (\(\times\)
		and the second	<del></del>	The state of the s	<del>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</del>							MODIFICATION/REPAIR Deepen
ļ		1	11/1	Line.	<del>)                                    </del>					ILE!		Other (Special
	100		<u> </u>									DESTROY (Describ
				<u> </u>						70 - WI	il	Procedures and Mai Under "GEOLOGIC
	1		200			<del></del>				J20'		PLANNED USES (
		**************************************	KEC	EIVE	Ŋ							DomesticX Put
		0	CI 1	3.20	100			WEST			AST	MONITORING
		i						^				TEST WELL CATHODIC PROTECTION
	! [	ENVI	RONMEN	CIVIENT ( TAL MAN	)F AGEMENT						J	HEAT EXCHANGE
	i 1				***************************************							DIRECT PUSH INJECTION
		!										VAPOR EXTRACTION
	! !	!								SOUTH	· · · · · ·	SPARGING REMEDIATION
	1	1			·····			Illustrate or De Fences, Rivers,	escribe Disto etc. and att	nnce of Well from Roc ach a map. Use addit CCURATE & COM	ids, Buildings, ional paper if	OTHER (SPECIFY)
	l .	1								EVEL & YIELD	<del>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</del>	ETED WELL
	; ;	i -	*					DEPTH TO F			ELOW SURFAC	
	! !	1			·			DEPTH OF S	TATIC 44			9-21-00
	t .	ł						WATER LEVE ESTIMATED	· · · · · · · · · · · · · · · · · · ·	,	E MEASURED . TEST TYPE .	ir lift
1		BORING _2		_(Feet)		÷ .		TEST LENGT	H	(Hrs.) TOTAL DRAV	DOWN N/A	(Ft.)
TOTAL D	EPTH OF	COMPLETED	WELL	23	(Feet)			* May not b	e represent	tative of a well's lo	ng-term yield.	
DEF		BORE-			C	ASING (S)				DEPTH	ANN	NULAR MATERIAL
FROM S	URFACE	HOLE -	TYPE (2		MATERIAL /	INTERNAL	GAUGE	SLOT S	11	FROM SURFACE	CE- BEN-	TYPE
Ft. to	o Ft.	(Inches)	SCREEN CON-	#     =	GRADE	DIAMETER (Inches)	OF WALL			Ft. to Ft.	MENT TONIT	E FILL FILTER PAC
0	240	13	+	+		1			$\dashv \vdash$	0 28	X	concret
	<del> </del>		$\Box$							28 61	X	chips
0	133	Х		ER	C F480	6	SDR-2	14		61 233		X pea gra
133	733	^n	X		C F480	6	SDR-2		$\dashv \vdash$		1	
	1											11000
		HMENTS (×	-) .		I, the unde	ersigned, ce	ertify that th			ON STATEMENT and accurate to the		knowledge and belief.
-	Geologi	c Log nstruction Diagr	am .		NAME			ELL DRI				
		nstruction Diagr sical Log(s)	G111		(PERS)	ON, FIRM, OR (	CORPORATION)	(TYPED OR PRINT	ED)	**		
		ter Chemical Ar	alyses		Monorco	2110	Penny	Lane	<del></del>	Nape	do CA	94559 STATE ZIP
-					ADDRESS	l de	Me.	1.JH			-10-00	43 <b>69</b> -746
ATTACH A	ADDITIONAL	INFORMATION,				·	ORIZED REPRESE	<del></del>		D	ATE SIGNED	C-57 LICENSE NUME
DWR 188 RF	EV. 11-97		IF A	DDITION	IAL SPACE IS	S NEEDED,	USE NEXT	T CONSECUT	TIVELY NU	JMBERED FORM		43 of 49

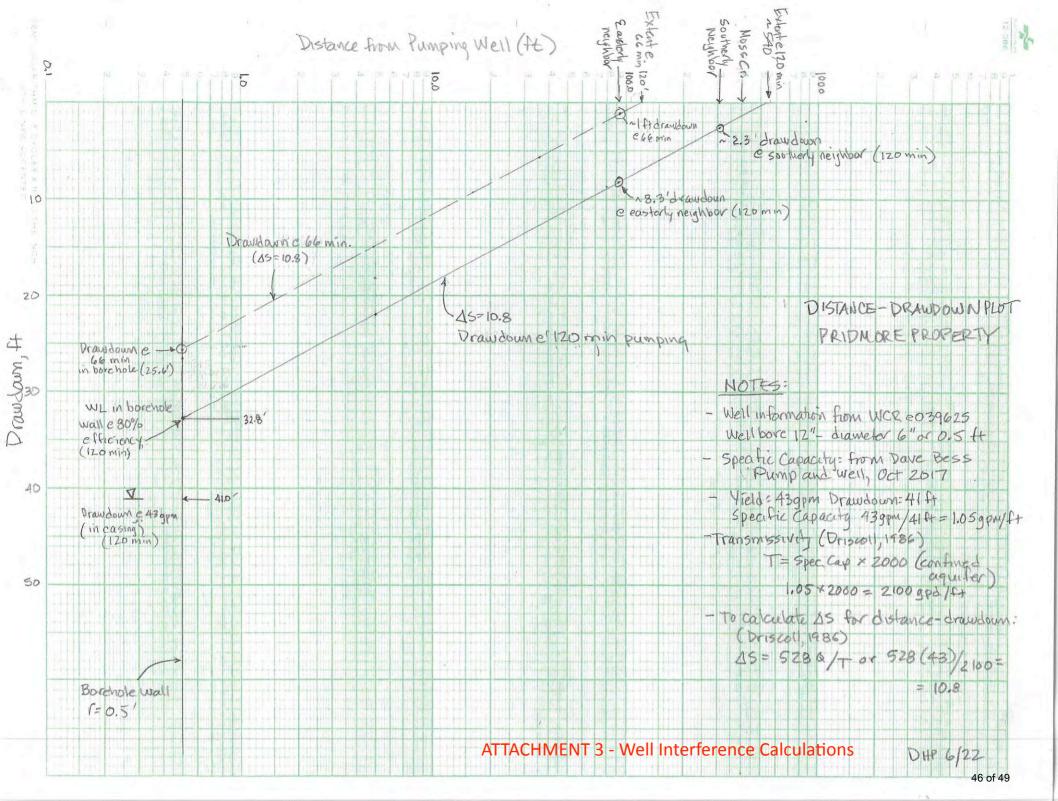
# **Environmental**

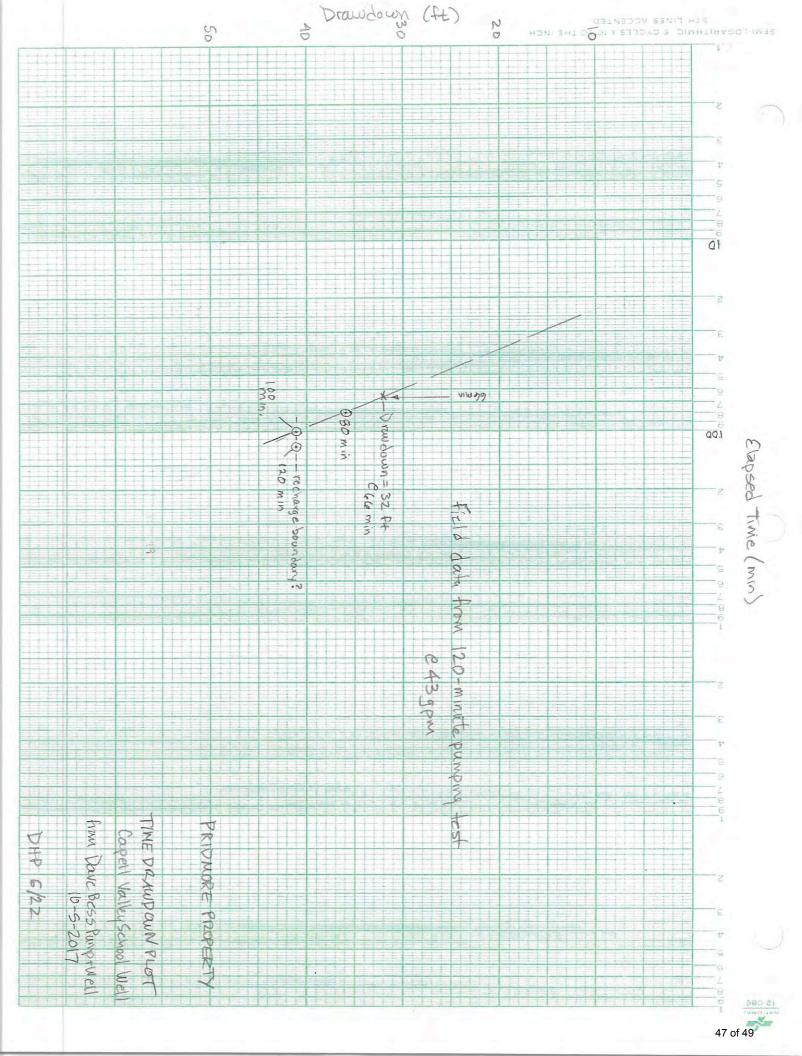
Cover Sheet

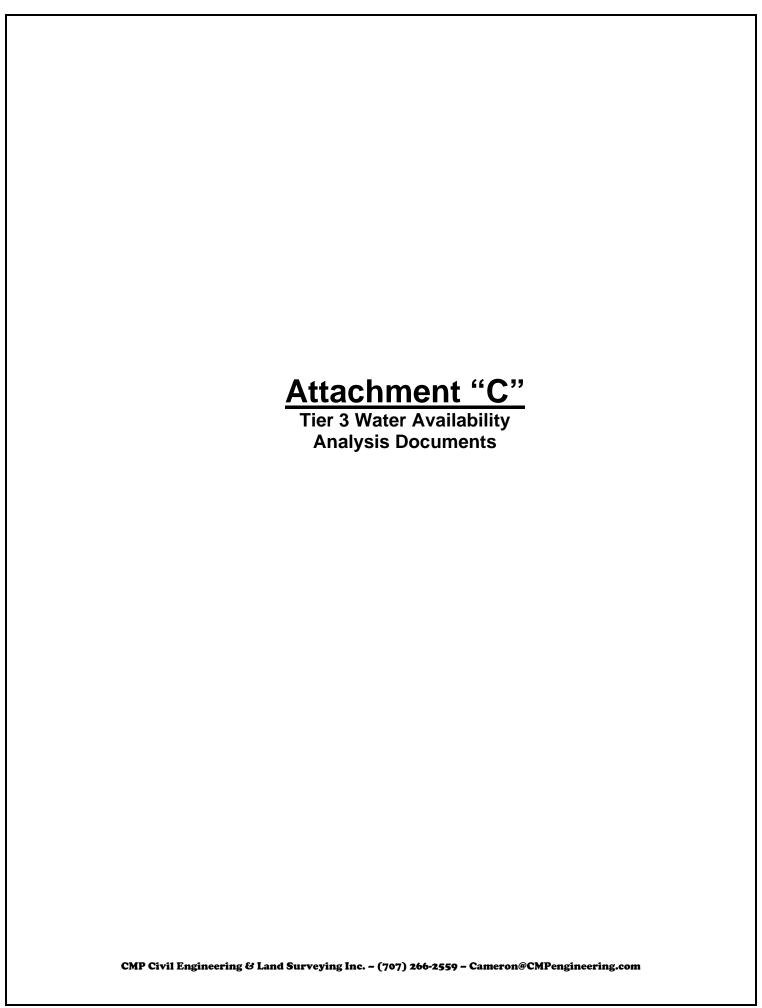
APN .	032 - 430 -010 -000
Permit #	
Program	Well
DocType	· WL
Street #	1191
Street Name	capell Vly Rd
Year	1996

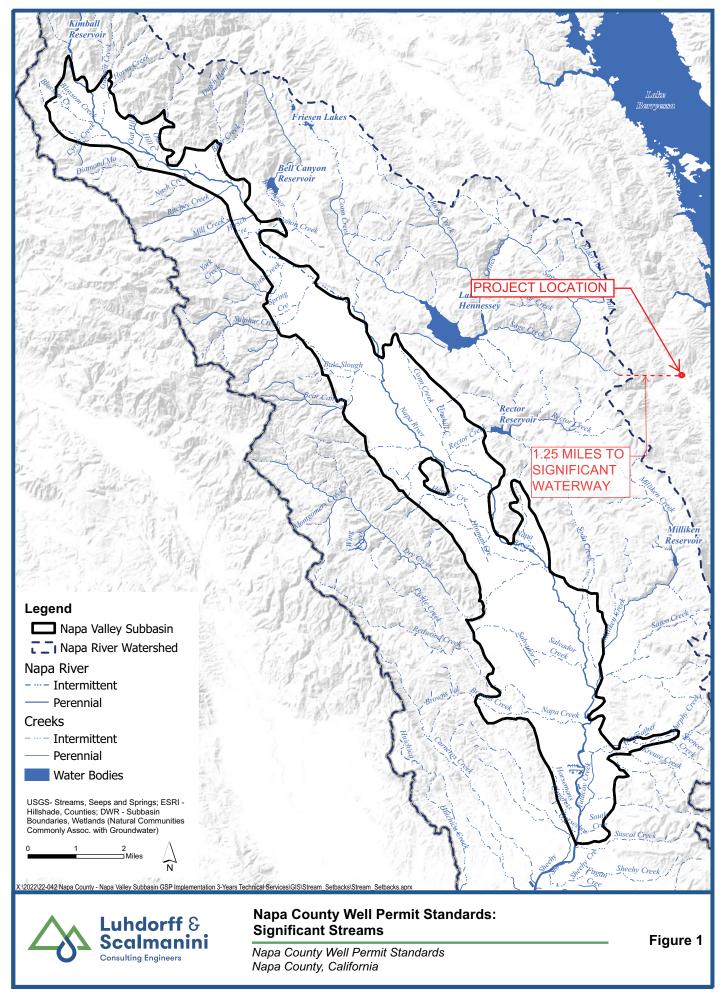


For Loca	al Requ	iiremer	nts			W	EL	L COM		IO	N REPOR	RT	- D W-R U				NOT FILL IN
Page 1									Instructio No			-	. 1 .	SIAI	F MELL	NO./S	TATION NO.
Owner's V	Vell No.	7-26	5_9/	 i			72.	-29-96.	. D.	1	6432	الم	LATITU	DE .	لـــا ك	<u>_</u>	LONGITUDE
Local Po	ermit As	ency 1	Van	a Co	)U1	ty Envi	ror	mental	Memt				1	1 1	<u> </u>	, -	1. 1 1 1 1
Perm	it No	42682	2			P	ermi	it Date	7-234	16	•				APN/T	RS/OT	HER
						c roc —		· · · · · · · · · · · · · · · · · · ·	÷	1		\$7.5 \$7.5	WELL	OWN	er —		
ORIENTATIO	ON (∠)	_X vi	ERTICA	۱ <u>ـــ</u>	_ н	ORIZONTAL _	/	ANGLE	(SPECIFY)	N	Vame						
DEPTH I	EDOM .	DÉPI	гн тс	FIRS	T W	ATER <u>18</u>	(Ft.	.) BELOW S	JRFACĘ /	: N	Mailing Addres	s <b>C</b>		120			
SURF	ACE	1		_		DESCRIPT			1/1/10	<u>-</u>	ITY	جي ت			······································	<b>Q</b>	IAIE ZIP
Ft. to	Ft.	<u> </u>		Descr	ibe i	naterial, grain	size,	color, etc.		+		7-	VELL L	OCAT	ION -		
0	18	3200	own	25 T x				Carried Control	· · · · · · · · · · · · · · · · · · ·	. T	ddress	some	177	·			
18	38					a grave	3			12	County	Mana	****				
38	60	·	ndet		-	hard	143%	patrice.	w" .		PN Book _0			Parce	1 01	Ô	
!		!	B.300,3183			113.11	,	, 1 m . c	3,4	Ţή,	ownship	. Range Bange		Section	n — —		
			200		<u></u>			·'= } ;	١.	L	o'hifuido'	<u> </u>	NORTH	Long	itude .		WES
1		1 18	2 <u>1</u>	,;			. 3	- ; ; -	ft.		DEG.	MIN. SEC			·	DEG.	MIN. SEC.
i		F	., ` <del></del>	3.	<u> </u>		٠ <u>٠</u>		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	F		NORTI	1			-X	ACTIVITY (ビ)ー
		1 1 ~ d	<del>,</del>	,	·				1,	-	The state of the s	Must				МОЕ	DIFICATION/REPAIR
<u> </u>			-	<u> </u>	٠		~ ) ;			-		A STREET, STRE	Windston I Z		,		Deépen
193s			- 4	;		1.5	<del></del>			┨		117	Personal Property lies	ing to a supplemental supplemen	HATTI BANKANIA		Other (Specify)
<del> </del>	1 3	1			, 25	<u>, , , , , , , , , , , , , , , , , , , </u>			<del></del>	┨			ELL		ASSESSED ASSESSED	1	
+	f	<u> </u>		<del></del> .		<u>\-</u>		harde.		1		search to be	Me has many		ng king		DESTROY (Describe Procedures and Material
1	******		<del>, }[</del>						·····	1,_	l il					L PL	Under "GEOLOGIC LOG" ANNED USE(S)
!			<u>,</u>					·····		VES.	110				EAST		(上) MONITORING
i i		I								1						1 -	ER SUPPLY
										]	35					1	Domestic
											Characteristic						Public
1		l L									** * * *	<b>1</b>				Ì	Irrigation
-											•	OREEK	* x				Industrial
ļ				8 31	4 3 7	11.11-cm				-		MEER	A & Money	raging and restar		-	"TEST WELL"
<u> </u>		· · · · · ·		ME	UE.	IVED				L		SOUTH				] -	ČATHODIC PROTEC-
<u>i</u>	·	<del></del>								I	llustrate or Descri	ibe Distance	of Well fro	m Land	marks	-	OTHER (Specify)
× .				Щij	U	7 1005	-			L	such as Roads, Bui PLEASE BE ACC	CURATE &	COMPLET	rE.		<u> </u>	
					DEPT	4				DF	RILLING ROLE	taren	ž vot				
	<u>-</u>	E	NVIR			. MANACEMLI	···			ME	THOD ROLL WATER	LEVEL &	YIELD	OF C			D WELL -
1	1					. 111110101011111	<u> </u>	****		DE	PTH OF STATIC						-29-96
-										,	STIMATED YIELD						
TOTAL DEI	TH OF I	BORING	60	i	_ (F	eet)					ST LENGTH2						
TOTAL DEI					•	AA.	eet)			ı	May not be repre						
	2 1		<del></del>			· · · · · · · · · · · · · · · · · · ·		LOXNO (O)				F		T			>6. G 77 7 7 . 7
DEPTI FROM SUF		BORE-	TV	PE (±	1893	145 - 47		ASING(S)	) 			DEF FROM S		1 P. W.	INNU	à	MATERIAL
1110141 001		HOLE DIA.				MATERIA	L/	INTERNAL	GAUG		SLOT SIZE	1110111 9	OIII AOL	-4 CÉ-	BEN-	- F.	(PE
Ft. to	Ft.	(Inches)	BLAN	SCREEN CON-	FILL PIPE	GRADE		DIAMETER (Inches)	OR WAI		IF ANY (Inches)	Ft. te	Ft.	MENT	TONITE		FILTER PACK (TYPE/SIZE)
0:	60	10	+		-						· · · · · ·	21%	11	$\frac{1}{X}$	( <u>'</u>	( - )	<b></b>
<u> </u>	2307	10	++	+	$\vdash$			1			<del> </del>	11	30	A		X*	concrete pea gravel
0	15		X	+	1	plast:	ic	5	SDR-2	7		1.2	.JU	-			hed Mrever
15	30	· · · · · · · · · · · · · · · · · · ·		X	$\vdash$	plast		5	SDR-2		,032			+			
					П					-				1		,	
-									,						7-		
A	TTACH	MENTS	( _	) —		7			· · · · · · · · · · · · · · · · · · ·		CERTIFICAT						
*******	Geologic I	_og				I, the	ındeı						urate to	the bes	-,		rledge\and belief.
	-	truction Dia	agram			NAME .	OF5-				WELL DRIL	LING			**	~1 # em "	
	Géophysic	al Log(s)					rers0	•		•	PED OR PRINTED)		***			a.	nteen
	Soil/Wate	r Chemical	l Anaiy	ses		ADDRESS		21:	10 Pen	ny	Lane		Napa			CA STATE	94559 ZIP
	Other	····				- []					111			2 <i>6</i> 3 <i>6</i> 4	n.	SIMIE	<del></del>
ATTACH ADD	ITIONAL II	FORMATI	ON. IF	IT EX	asts	Signed	WELI	DRILLER/AUTHO	RIZED REPRES	SENT	ATIVE			10-2			439-746 C-57 LICENSE NUMBER
OWR 188 REV. 7-	90	**	IF /	\DD!T	ION	AL SPACE	IS N	EEDED, U	SE NEXT	cö	NSECUTIVELY	NUMBERÊ					











Nicholas F. Bonsignore, P.E. Robert C. Wagner, P.E. Paula J. Whealen Martin Berber, P.E.
Patrick W. Ervin, P.E.
David P. Lounsbury, P.E.
Vincent Maples, P.E.
Leah Orloff, Ph.D, P.E.
David H. Peterson, C.E.G., C.H.G.
Ryan E. Stolfus

#### **MEMORANDUM**

**To:** Cameron Pridmore. P.E.

**From:** David H. Peterson, CEG, CHg

**Date:** July 24, 2023

**Re:** Supplemental Tier 3 Water Availability Analysis

**Pridmore Family - Capell School Lodging Project** 

1191 Capell Valley Road, Napa, CA

This memorandum summarizes the supplemental Tier 3 water availability analysis performed for the proposed Capell School Lodging Project, located at 1191 Capell Valley Road, Napa, California. The property is located on the northeast side of Capell Valley Road and about 0.8 miles northwest of the intersection of Highways 121 and 128 in eastern Napa County, as shown on the attached *Site and Well Location Maps*, **Figures 1 and 2**.

We previously performed a Tier 2 analysis for the project, summarized in a February 8, 2023 report. The purpose of that study was to assess the impacts of pumping by the project well on neighboring wells located within 500 feet. We understand Napa County has accepted the Tier 2 study. However, we understand the County will now also require a Tier 3 analysis of the potential effects of groundwater pumping on nearby surface waters.

#### **Project Description**

A description of the project and the local hydrogeologic setting were presented in our Tier 2 analysis report and we have limited the description in this supplemental study to data pertinent to the Tier 3 analysis. Water supply for the project will be from an existing well on the property, referred to as the Project Well. Total domestic and landscaping water demand for the project is calculated by CMP Engineering and Surveying at 1,042,652 gallons per year, or 3.20 acre-feet per year (AFY). The estimated annual water demand equates to about 2,857 gallons per day, or at the tested pumping rate of 43 gallons per minute (gpm), about 66 minutes of daily pumping from the Project Well.

The *Well Location Map* from CMP and the Tier 2 study is shown on **Figure 3**. An intermittent stream, informally designated Pridmore Creek, is about 500 feet north of the Project Well and generally bounds the northerly margin of the subject property. South of the property and Capell Valley Road is Oak Moss Creek, shown on the U.S. Geological Survey Capell Valley 7.5-

Cameron Pridmore July 24, 2023 Page 2

minute quadrangle as an intermittent (blue-line) creek. Oak Moss Creek is about 400 feet south-southwest of the Project Well at its nearest point.

#### **Project Well**

The local geologic setting is shown on **Figure 4** and the well completion report (WCR e039625) for the Project Well is included as **Attachment 1**. The well was drilled in June-July 2006 by Huckfeldt Well Drilling Inc. of Napa, California. The initial wellbore was drilled to a total depth of 260 feet. The well log indicates that clay alluvium was encountered to a depth of 54 feet, underlain by clay, shale and sandstone bedrock of the Great Valley Sequence. The wellbore was competed with a 250-foot deep, 6-inch diameter casing. As constructed, the well perforations extend from a depth of 70 to 170 feet and 190 to 250 feet, entirely within the Great Valley Sequence mélange unit. A bentonite and cement seal was placed in the upper 55 feet of the well, which extends through the surface alluvial units. Based on the reported 54-foot thickness of the alluvium on the log, it appears that the 55-foot well seal completely sealed off the alluvium from the underlying Great Valley Sequence bedrock units.

The WCR indicates that groundwater was first encountered at a depth of 70 feet, within the Great Valley Sequence. The static water level subsequently rose to a depth of 15 feet, indicating that groundwater is semi-confined or confined in the Great Valley Sequence bedrock.

#### Tier 3 – Analysis of Groundwater-Surface Water Interaction

The subsurface conditions in the site vicinity are shown graphically on Cross Section A-A' on **Figure 5.** As shown, Pridmore Creek lies about 500 feet north of the Project Well and Oak Moss Creek lies about 400 feet to the south. Our field observations and review of the Project Well log indicate that Pridmore Creek is likely underlain by about 30 to 35 feet of clay alluvium. To the south, field observations indicate that alluvium is generally exposed in the bed and banks of Oak Moss Creek, although bedrock of the Great Valley Sequence was also observed to be locally exposed in the bed and lower banks just west of APN 032-430-010. Based on interpretation from our cross section, alluvium generally underlies the bed of Oak Moss Creek to a depth of about 10 feet.

In the County's Approach for Evaluating the Potential Effects of Groundwater Pumping on Surface Water Flows (October 11, 2013), it is noted that "Any potential for direct impacts to surface water courses resulting from groundwater pumping relies on a physical connection between the pumped groundwater system and the surface water course." Review of the well log for Project Well indicates that it penetrates 54 feet of clay alluvium, underlain by sandstone and shale bedrock strata of the Great Valley Sequence. The well was constructed with a 55-foot-deep grout and cement seal, which seals off the alluvium. Since water was first at a depth of 70 feet, groundwater from the Project Well appears to be confined in bedrock units at depth within the Great Valley Sequence. It therefore appears unlikely that groundwater at that depth is in direct physical connection with either creek.



The calculated extent of lateral pumping influence from the Tier 2 analysis was also considered to assess potential effects of pumping on the two watercourses. Based on time-drawdown data taken from a 2017 pumping test by Dave Bess Pump & Well, pumping for 66 minutes (the average daily pumping demand for the project) would create a zone of lateral pumping influence extending about 120 feet from the Project Well. Given that the two watercourses are about 400 and 500 feet away, a typical pumping cycle would not be anticipated to directly reach either creek. Since an average daily pumping cycle is estimated at only 66 minutes, it is also expected that the water level near the Project Well would recover between pumping cycles.

As an additional screening tool, the U.S. Geological Survey stream depletion program STRMDEPL08 (Reeves, 2008) was used to assess if the short pumping cycles from the Project Well had a potential for stream depletion. Use of STRMDEPL08 has limitations, since it assumes that the well pumps from a laterally infinite and homogeneous aquifer of uniform thickness. However, as discussed, the sheared mélange bedrock beneath the site is probably not laterally uniform. Additionally, STREMDEPL08 only calculates depletion in full-day increments. STRMDEPL08 estimates stream depletion under four alternate scenarios:

- 1. Fully penetrating stream with no streambed resistance (Jenkins, 1968)
- 2. Fully penetrating stream with streambed resistance (Hantush, 1965)
- 3. Partially penetrating stream with streambed resistance (Hunt, 1999)
- 4. Partially penetrating stream in an aquitard overlying a pumped aquifer (Hunt, 2003)

For our screening analysis, Scenario 4 - Partially penetrating stream in an aquitard overlying a pumped aguifer (Hunt, 2003) was used, since both creeks appear to lie within clay alluvium (aguitard) overlying a confined, fractured/sheared rock aguifer at depth. For inputs to the program, a transmissivity of 2,100 gallons/day/ft (converted to 281 ft/ft/day), derived in the Tier 2 analysis was used. In addition, the storage coefficient of 0.014 for the bedrock aquifer was calculated using information from the Tier 2 study (pumping duration, lateral extent of pumping influence, and transmissivity) and an online inverse Theis Equation Calculator developed by the New Mexico Office of the State Engineer (2017; see **Attachment 2**). Hydraulic conductivity (0.01 to 0.001 ft/day) and specific yield (0.01) for the clayey alluvial aquitard were obtained from Tables F-2 and F-4 of the Napa County WAA Guidance Document. Aguitard thickness and channel dimensions were estimated from the cross section on Figure 5. For the purposes of this analysis, a full day of pumping was used as an input, although as previously discussed, actual pumping cycles would be of much smaller duration. Based on these inputs and an assumed distance of 400 feet (i.e., Oak Moss Creek), STRMDEPL08 calculates that no depletion would occur after one full day of pumping at 43 gpm. A copy of the STRMDEPL08 input and output files is included as Attachment 3.

From this screening analysis and the previously described approaches to analyzing to the potential for stream depletion, it appears that the limited duration pumping cycles required for the project would not directly impact nearby streams.



#### **Discussion and Conclusions**

Analysis of potential streamflow depletion using the data from the 2017 well test by Dave Bess Pump & Well and our estimates of lateral pumping influence for the Tier 2 study indicated that pumping from the Project Well would not reach Pridmore Creek or Oak Moss Creek during a typical daily pumping cycle. Using default inputs from the Napa County WAA Guidelines and USGS program STRMDEP08, a longer period (i.e. a full day) of pumping from the Project Well would also not be expected to have a direct effect on Pridmore or Oak Moss Creeks. At the planned pumping rate and daily project water demand, direct depletion effects on Pridmore Creek or Oak Moss Creek from pumping the Project Well appear unlikely.

We trust this supplemental memorandum provides the information requested by the County of Napa. Please contact us if you have questions about the findings or require additional information.

### Figures and Attachments

Figures 1 and 2 – Site and Well Location Maps

Figure 3 – Well Location Map, from CMP Engineering (2022)

Figure 4 - Vicinity Geologic Map

Figure 5 – Cross Section A-A'

Attachment 1 – Project Well Log

Attachment 2 – Coefficient of Storage Calculation (New Mexico OSE, 2017)

Attachment 3 – USGS STRMDEPL08 files

#### References

California Department of Water Resources, 2020, Well Completion Report Map Application: <a href="https://dwr.maps.arcgis.com/apps/webappviewer/index.html?id=181078580a214c0986e2da28f86">https://dwr.maps.arcgis.com/apps/webappviewer/index.html?id=181078580a214c0986e2da28f86</a> 23b37

California Department of Water Resources, 2022, Water Data Library, online map application with groundwater level and water quality data: <a href="http://wdl.water.ca.gov/waterdatalibrary/">http://wdl.water.ca.gov/waterdatalibrary/</a>

Driscoll, F.G., 1986, Groundwater and Wells: Johnson Division, St. Paula Minnesota, 1,089p.

Groundwater Resources Association, 2004, Low Yield Aquifer Testing Seminar: notes from short course presented April 26, 2004, Walnut Creek, CA.



Johnson, A.I., Specific Yield – Compilation of Specific Yields for Various Materials in Hydrologic Properties of Earth Materials: U.S. Geological Survey Water-Supply Paper 1662-D, 80p.

Kunkel, F. and Upson, J.E., 1960, Geology and Ground Water in Napa and Sonoma Valleys, Napa and Sonoma Counties, California: U.S. Geol. Survey Water-Supply Paper 1495, 252p., with illustrations.

Napa County, 2005, Napa County Baseline Data Report, Chapter 16, Groundwater Hydrology: baseline study for County General Plan update, Version 1, November 2005.

Napa County, 2015, Water Availability Analysis (WAA) – Guidance Document: Adopted May 12, 2015, 42p.

Napa County, 2013, Approach for Evaluating the Potential Effects of Groundwater Pumping on Surface Water Flows and Recommended Well Siting and Construction Criteria: Final Technical Memorandum dated October 11, 2013, 43p.

New Mexico Office of the State Engineer, 2017, OSE Inverse Theis Calculator: online application at: https://www.ose.state.nm.us/Hydrology/Theis/index.html

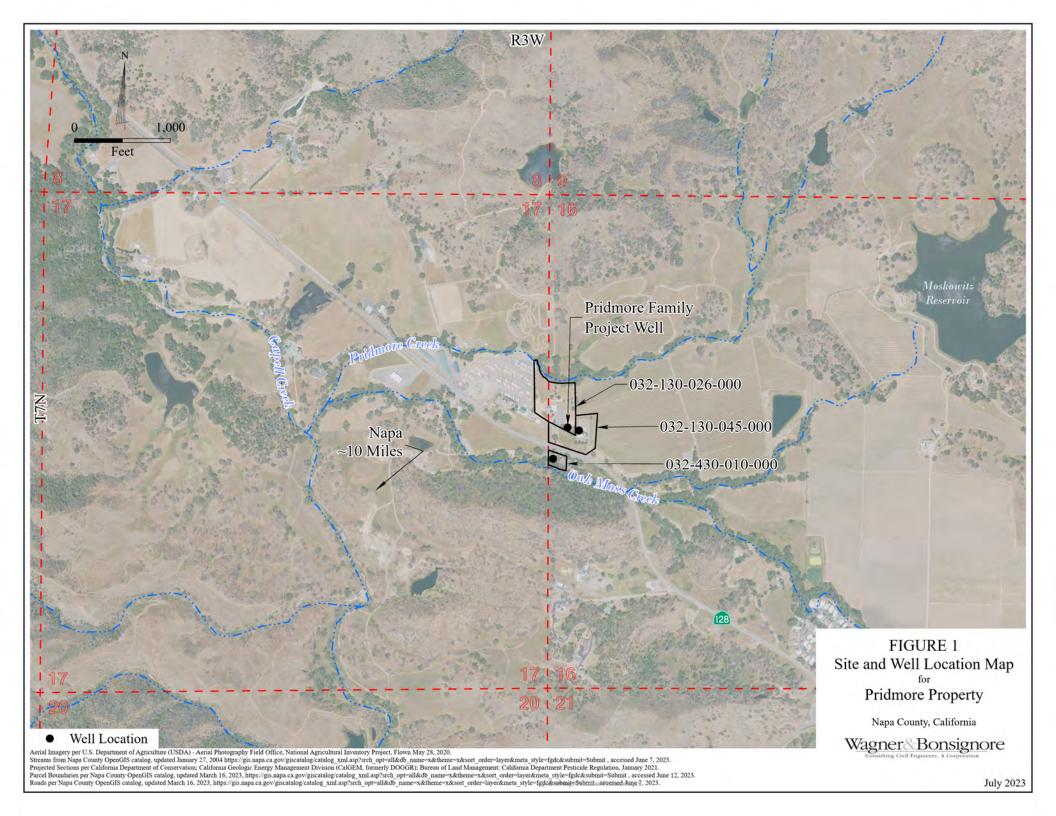
Reeves, H.W., 2008, STRMDEPL08-An Extended Version of STRMDEPL with Additional Analytical Solutions to Calculate Streamflow Depletion by Nearby Pumping Wells: U.W. Geological Survey Open-File Report 2008-1166. 32p.

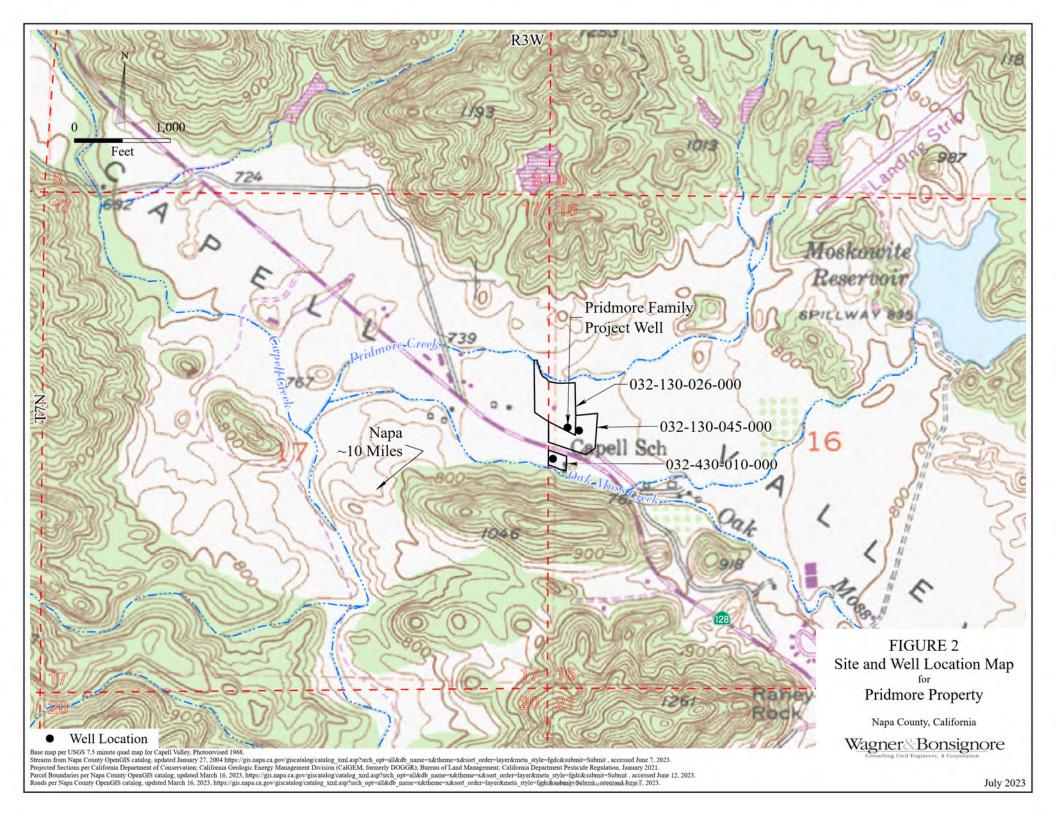
Thomasson, H.G., Olmsted, F.H., an LeRoux, E.F., 1960, Geology, Water Resources and Usable Ground-Water Storage Capacity of Part of Solano County, California: U.S. Geological Survey Water-Supply Paper 1464, 711p. (p.220-223; Hydraulic Characteristics Estimated from Pump-Efficiency Tests).

- U.S. Geological Survey, 2022, National Water Information Service, online surface and groundwater data: <a href="https://waterdata.usgs.gov/nwis">https://waterdata.usgs.gov/nwis</a>
- U.S. Geological Survey, 2022, STRMDEP08 An Extended Version of STRMDEPL with Additional Analytical Solutions to Calculate Streamflow Depletion by Nearby Pumping Wells: Water Resources Ground Water Software, Michigan Water Science Center: online application: <a href="https://mi.water.usgs.gov/software/groundwater/strmdepl08/">https://mi.water.usgs.gov/software/groundwater/strmdepl08/</a>

Wagner & Bonsignore Consulting Civil Engineers, 2022, Tier 2 Water Availability Analysis, Pridmore Family – Capell School Lodging Project, 1191 Capell Valley Road, Napa, CA: unpublished consultants report dated February 8, 2023, 19p.







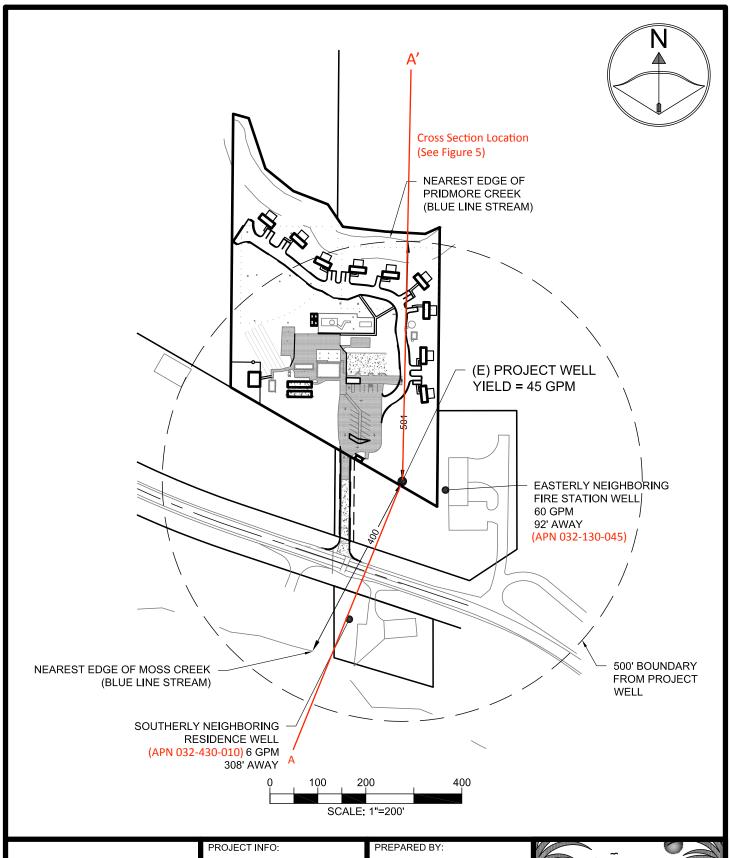
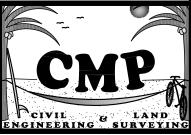


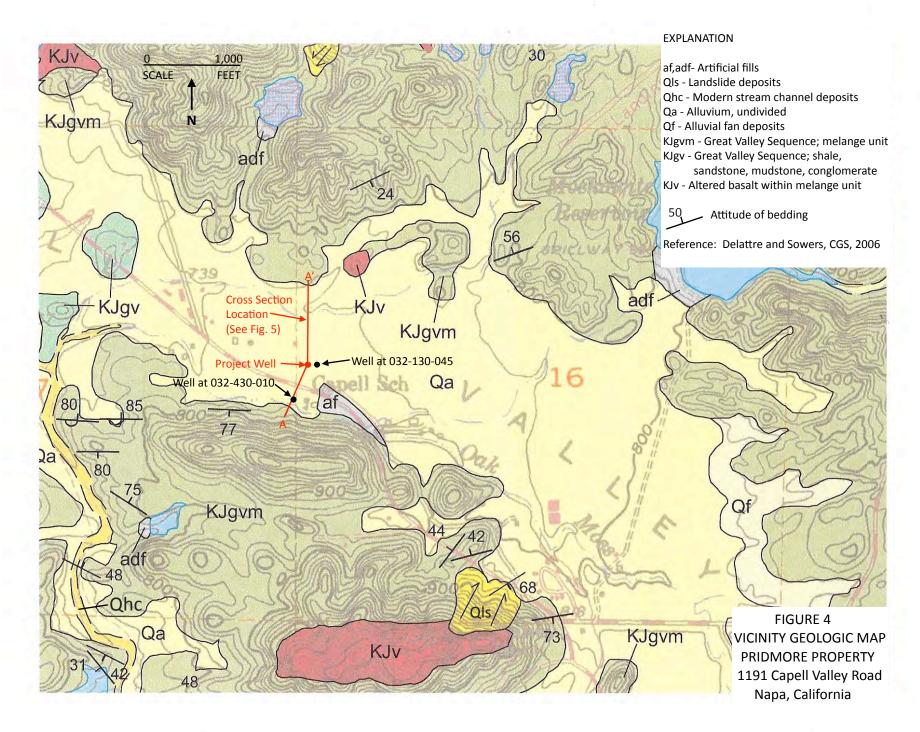
FIGURE 3
WELL LOCATION MAP

PRIDMORE PROPERTY (FORMALLY CAPELL VALLEY SCHOOL) 1191 CAPELL VALLY ROAD NAPA, CA 94558 032-130-026 CMP CIVIL ENGINEERING & LAND SURVEYING INC. 1607 CAPELL VALLEY ROAD NAPA, CA 94558 (707) 266-2559

P #: 00055 DATE: 04/05/2022



SHEET: 1 OF 1



Text

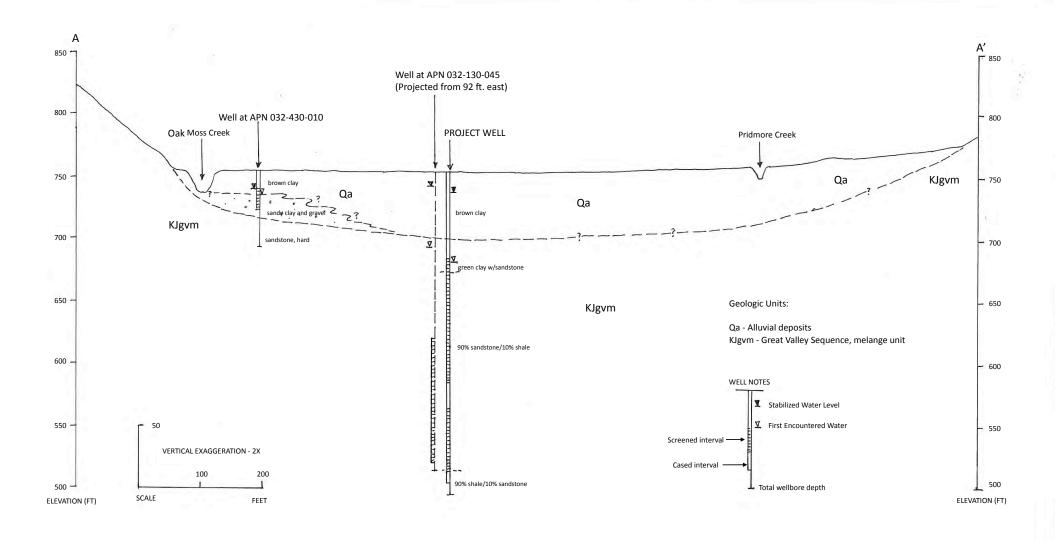


FIGURE 5 CROSS SECTION A - A' PRIDMORE PROPERTY 1191 Capell Valley Road Napa, California

#### ATTACHMENT 1 - PROJECT WELL

**ORIGINAL** File with DWR STATE OF CALIFORNIA

#### **COMPLETION** REPORT Refer to Instruction Pamphlet WELL

Page 1 of 1

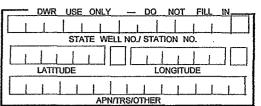
Owner's Well No. 1-'06

No. e039625

, Ended 7/13/2006 Date Work Began 6/29/2006

Local Permit Agency Napa County Environmental Mgmt
Permit No. E06-01092 Permit Date 6/2

Permit Date 6/28/2006



Perm	II No. =	Permit Date 6/28/2006	
		GEOLOGIC LOG	WELL OWNER
ORIENTA'	TION (≰)	VERTICAL HORIZONTAL ANGLE(SPECIFY)	Name Welley Wallied School Dratito
<u> </u>		DRILLING ROTARY FLUID BENTONITE	Mailing Address Id Colling On Avenue
DEPTH	FROM	DESCRIPTION	Qapa 44558
Ft. to		Describe material, grain, size, color, etc.	CITY STATE ZIP
0	54	BROWN CLAY	Address 1191 Capell Valley Road
54	80	GREEN CLAY WITH SANDSTONE	City Napa CA
80	250	90% SANDSTONE/ 10% SHALE	County Napa
250	260	90% SHALE & CLAY/ 10% SANDSTONE	, · ·
			APN Book 032 Page 130 Parcel 026
<del>                                     </del>			Township Range Section
			Latitude I I I DEG. MIN. SEC. DEG. MIN. SEC.
			LOCATION SKETCH————————————————————————————————————
<b> </b>			NORTH   ✓ NEW WELL
<b></b>		<u> </u>	MODIFICATION/REPAIR
<u> </u>			— Deepen — Other (Specify)
<b> </b>			REEN Outer (specify)
			DESTROY (Describe
			DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG"
-			PLANNED USES(∠)
			WATER SUPPLY Domestic  Public
<del>  -</del>		· · · · · · · · · · · · · · · · · · ·	SCHOOL SOMESTIC TO Public Wingation Industrial
			MONITORING
			WELL TEST WELL.
			CATHODIC PROTECTION
			7. 19. 1
			DIRECT PUSH
			VAPOR EXTRACTION
			SPÁRGING
			SOUTH REMEDIATION  Illustrate or Describe Distance of Well from Roads, Buildings,
			Hinstrate or Describe Distance of wen from Rodax, Biniangs, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.
			WATER LEVEL & YIELD OF COMPLETED WELL DEPTH TO FIRST WATER 70 (Ft.) BELOW SURFACE
			DEPTH OF STATIC WATER LEVEL 15 (Ft.) & DATE MEASURED 7/13/2006
<u></u>		onnya 260	ESTIMATED YIELD * 45 (GPM) & TEST TYPE AIR LIFT
		ORING 260 (Feet)	TEST LENGTH 3 (Hrs.) TOTAL DRAWDOWN N/A (FL)
TOTAL DE	PTH OF C	OMPLETED WELL 250 (Feet)	May not be representative of a well's long-term yield.
	<del></del>		

DEF		BORE.	CASING (S)									EPTH		ANNULAR MATERIAL				
FROM SU	FROM SURFACE HOLE DIA. (Inches)		T ¥	YPI	<u> (</u>	) JPE	MATERIAL /	INTERNAL DIAMETER	GAUGE OR WALL	SLOT SIZE IF ANY	FROM	SURF	ACE	CE-	BEN-		PE FILTER PACK	
Ft. to	FL	(mones)	BLANK	SCREEN	CON-	님	GRADE	(Inches)	THICKNESS	(Inches)	Ft	to	Ft.	MENT (✓)	TONITI	FILL ( <u>v</u> )	(TYPE/SIZE)	
0	260	12									0		5	✓			CONCRETE	
											5	; <u> </u>	22		1		GROUT	
0	70		<b>V</b>				PVC F480	6	SDR-21		22	! ]	55	✓			CEMENT	
70	170			<b>√</b>			PVC F480	6	SDR-21	.032	55	; ]	250			1	#6 SAND	
170	190		~	_			PVC F480	6	SDR-21			1						
190	250			1			PVC F480	6	SDR-21	.032		1						

ATTACHMENTS (∠)	I <del> </del>		CERTIFIC	CATION STATEMENT —		·····
Geologic Log				ate to the best of my knowledge an	d belief.	
Well Construction Diagram	NAME HUCKFE	<u>L'DT WELL DI</u>	RILLING, INC.			
Geophysical Log(s)			TION) (TYPED OR F	PRINTED)		
- Soil/Water Chemical Analysis	2110 Penny Lan	e 1		Napa	CA	94559
Other	ADDRESS	Um 1	111.10 0/Al	CITY	STATE	ZIP
ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.	Signed		MARKANT.	07/14/		9-746
ATTACH ADDITIONAL INFONMATION, IF IT EXISTS.	WELL DRILLE	R/AUTHORIZED 1	REPRESE TATIVE	DATE SIG	GNED C-5	7 LICENSE NUMBER

## CAPELL SCHOOL WELL YIELD

#### DAVE BESS PUMP & WELL

LIC.# C-57-C-10 487027

WATER WELL TEST REPORT# W-17-039 1115 MT GEORGE AVE. NAPA, CALIF. 94558 707-226-2539 / 253-0574

LOCATION (well address): 1191 Capell Vallev Rd Napa CA Date 050ct2017
TEST REQUESTOR: Gil Pridmore

#### SURFACE INSPECTION

CASING DIA. 6" pvc EST. AGE OF WELL 12 Years (Per Well Log) DEPTH OF WELL 250' (Per Well Log) SANITARY SEAL (functional) PIPING SYSTEM (functional) ELECTRICAL SYSTEM (functional) PRESSURE TANKS (functional) WELL SIZE OF PUMP 2 (HP)

OPERATING VOLTS: 239 AMPS: R: 2.8 B: 9.5 Y:P 10.0

#### FLOW TEST DATA

METHOD OF TEST: 2 HOUR OPEN FLOW DISCHARGE TEST USING THE INSTALLED PUMP AND EXISTING EQUIPMENT. (TEST EQUIPMENT USED), 2" FLOW METER, 2" THROTTLING DISCHARGE VALVE, 0/200 PRESSURE GAGE AND A POWERS WELL DEPTH STATIC METER.

TIME	RATE (GPM)	WATER LEVEL
14:00	50	20ft
15:20	43	56ft
15:40	43	61ft
16:00	43	61ft

STATIC LEVEL PRIOR TO TEST <u>20</u> FT STATIC LEVEL @ END OF TEST <u>61</u> FT TOTAL DRAW DOWN DURING THIS TEST WAS <u>41 ft</u> (AVG.)GALLONS PER MIN. <u>44.75</u> FOR <u>2</u> HOURS OF TESTING.

#### GENERAL COMMENTS

Well and well equipment in working order @ time of testing. The well fills a storage tank and is pressurized from the storage tank with 2 Goulds Booster pumps One ¾ HP (HB707) and 1 lhp (HB2510). Pressure Tanks are showing signs of deterioration (Rusting) and should be replaced. It seems that all controls are low voltage. The water is treated with a Culligan system, it is unknown if its operational or being serviced. Some information was taken from the well completion report Dated 6/28/2006 Log #e039625. Pump Depth is unknown at this time. Flow Meter Installed after the Booster pumps reads 5155799 Gallons.

Disclaimer: The data and conclusions provided herein are based upon the best information available to this company using standards and accepted practices of the water well drilling industry. However, well yield conditions are subject to dramatic changes in short periods of time due to usage and recharging of aquifers, etc. Therefore, the data and conclusions taken during this test are only valid of the day of the test and should not be relied upon to predict either the future quantity or quality of the well. This company makes no warranties either expressed or implied as to future water production and expressly disclaims and excludes any liability for consequential or incidental damages arising out of the breach of any expressed or implied warranty of future water production or out of any future use reported by the customer.

#### **ATTACHMENT 2**

### **OSE Inverse Theis Calculator**

This application allows one to input 5 of the following 6 parameters to predict the 6th (with the exception of Transmissivity): Transmissivity (select units of gpd/ft or ft²/d); Storage Coefficient; Time (years) since the beginning of pumping; pumping rate (select units of gpm or acre-feet/yr); Distance (select units of feet or miles) from the pumping well; and Drawdown (ft) at the given distance. You cannot solve for Transmissivity because for most sets of parameter values, there is not a unique solution for Transmissivity.

Please select the parameter to be determined and enter the the other parameter values:

Calculate The Store	nge is 0.0140	
O Drawdown (feet)	0.01	
<ul><li>Distance</li></ul>	120	• feet • miles
O Time	0.046	○years • days
<ul><li>Pumping Rate</li></ul>	43	ogpm oacre-ft/yr
<ul><li>Storage Coefficient</li></ul>		
Transmissivity	2100	$\odot$ gpd/ft $\bigcirc$ ft <sup>2</sup> /d

#### Notes:

- If using Internet Explorer, you may need to click the button at the bottom of the window to "Allow blocked content". Another option is to change your IE security settings to "Allow active content to run in files on My Computer".
- If you have problems or detect errors with this program, please contact the webmaster.
- Disclaimer: This application uses numerical algorithms to estimate output values. OSE has attempted to ensure that these algorithms and code are error free, but makes no such guarantee. The user should attempt to verify the results. Anyone utilizing the output of this program does so at their own risk.
- ©2017 New Mexico Office of the State Engineer, All Rights Reserved.

1 of 1 6/29/23, 11:19 AM

USGS - science for a changing world

#### ATTACHMENT 3 - STRMDEPL08

**Fully penetrating stream** 

USGS Home Contact USGS Search USGS

#### Michigan Water Science Center

Michigan Water Science Center ◆ Water Resources Ground Water Software

The Web-Based STRMDEPL08 evaluates four analytical solutions that simulate streamflow depletion by a nearby pumping well. It is based on STRMDEPL08 (Reeves, 2008) and the earlier STRMDEPL (Barlow, 2000). These two earlier programs are written in Fortran, require text input files, and produce tabular output. The web-based version was written to provide an easier interface to the analytical solutions with more convenient units and simplified output. (View more...)

#### **Calculate Streamflow Depletion by Nearby Pumping Well**

with no streambed resistance (Jenkins, 196		with streambed resistance (Hantush, 1965)	
Distance (ft):	Distance (ft):		
Transmissivity (ft2/day):	Transmissivity (ft2/day):		
Storage Coefficient:	Storage Coefficient:		
Pumping Rate (gpm):	Streambed Leakance (ft):		
Days of Pumping:	Pumping Rate (gpm):		
	Days of Pumping:		

# Partially penetrating stream with streambed resistance (Hunt, 1999)

Fully penetrating stream

Distance (ft):	
Transmissivity (ft2/day):	
Storage Coefficient:	
Streambed Conductance (ft/day):	
Pumping Rate (gpm):	
Days of Pumping:	

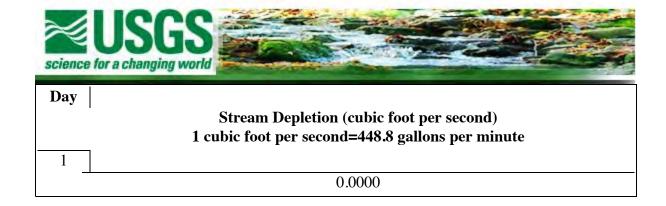
Units used

- ft: foot
- ft2/day: square foot per day
- gpm: gallons per minute
- ft/day: foot per day
- Note, 1 cubic foot per second = 448.8 gallons per minute

#### Partially penetrating stream in an aquitard overlying a pumped aquifer (Hunt, 2003)

1	,
Distance (ft):	400
Transmissivity (ft2/day):	281
Storage Coefficient:	0.014
Specific Yield of Aquitard:	0.01
Hydraulic Conductivity of Aquitard (ft/day):	0.01
Stream Width (ft):	30
Thickness of Aquitard (ft):	30
Distance from Streambed to Bottom of Aquitard (ft):	10
Pumping Rate (gpm):	43
Days of Pumping:	1

1 of 2 7/10/23, 11:02 AM



1 of 1 7/10/23, 11:03 AM